

FIELD BOOK

S 1133

PLEASE RETURN TO
GEAUGA COUNTY ENGINEER
COURT HOUSE
CHARDON, O.
PHONE 250-X

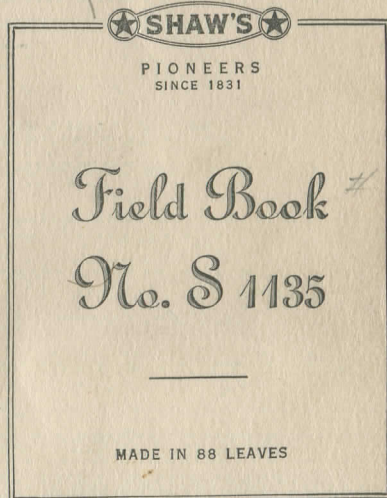
GARRIS CORNERS N. ROAD

42 UNDER ROAD

{ Topography P- 1-17
{ Check Levels P. 19-21
{ Cross-Sections P. 22-32

Mosley Rd. Eng. S.P. #528
Pg 42

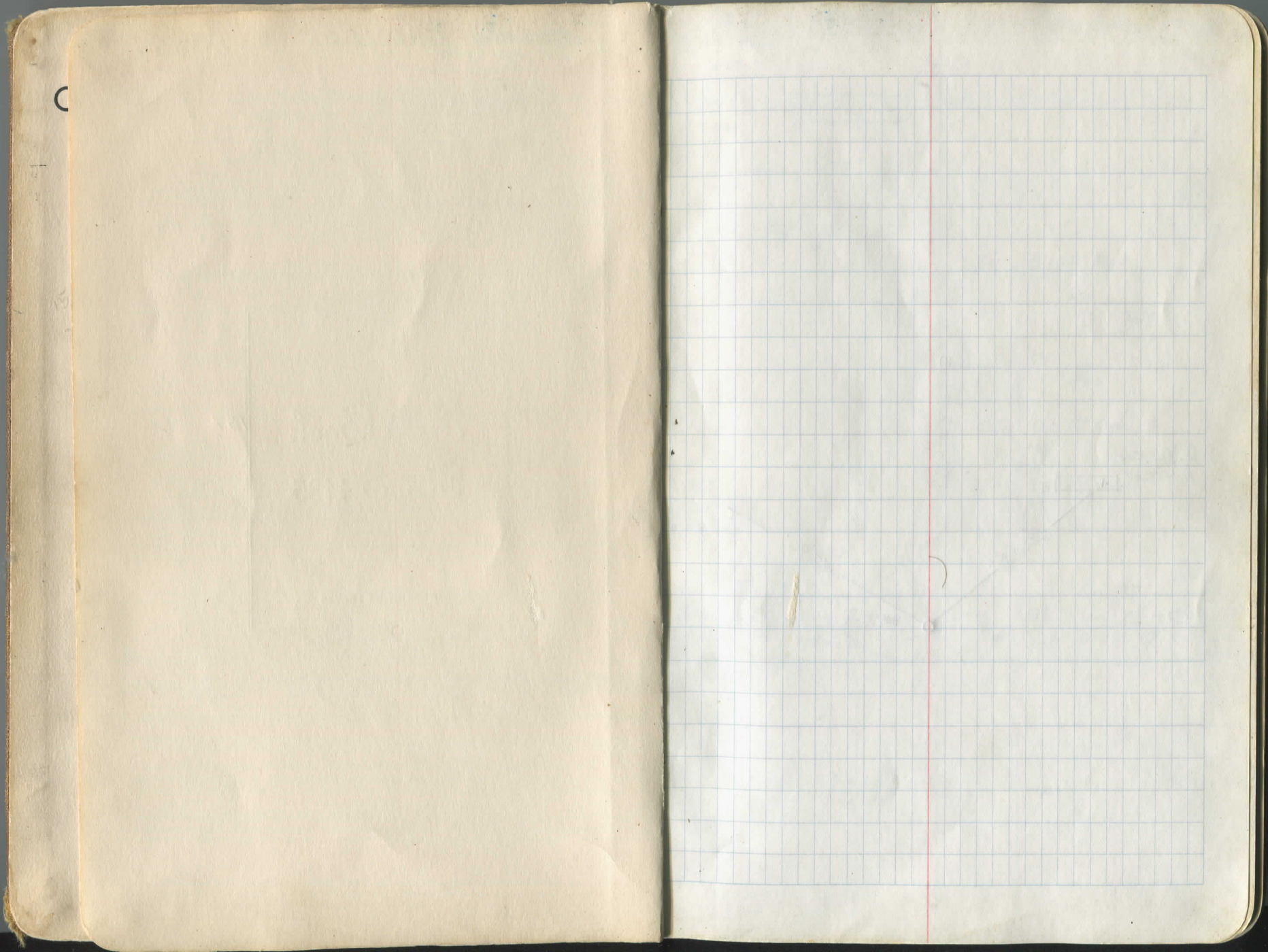
Thompson Ctr. East. pg 52



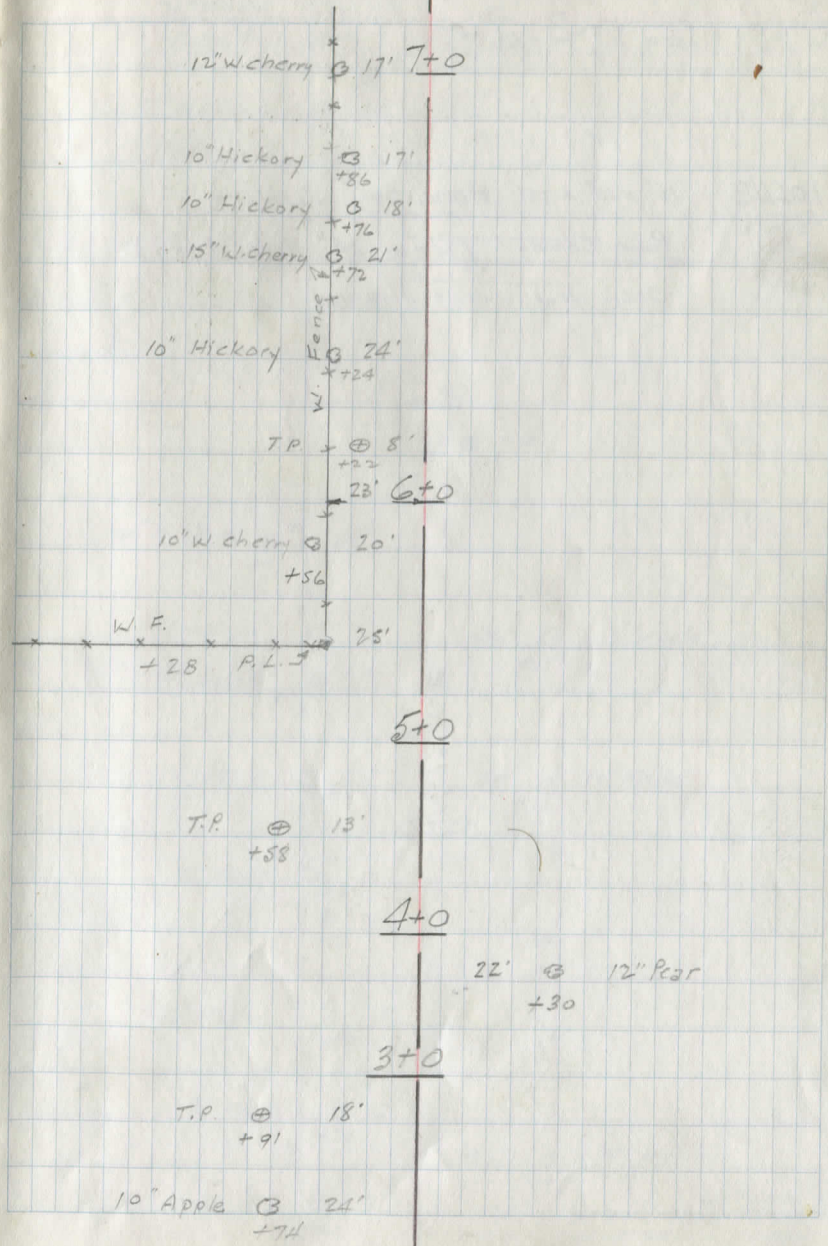
A Product of Wilson-Jones Co.
Made in U. S. A.

THOMPSON CTR. EAST SEC G-H
Soil Samples Pg 60

56-End



N-2°-15'-E



14+41 16'x12" Corr. I.P. Culvert +
 Eliminate Culvert & use pipe at Sta 43+48^{II}
 (Side Rd. Culvert)

S. & W
 S.W. Root
 12" Maple

29.94

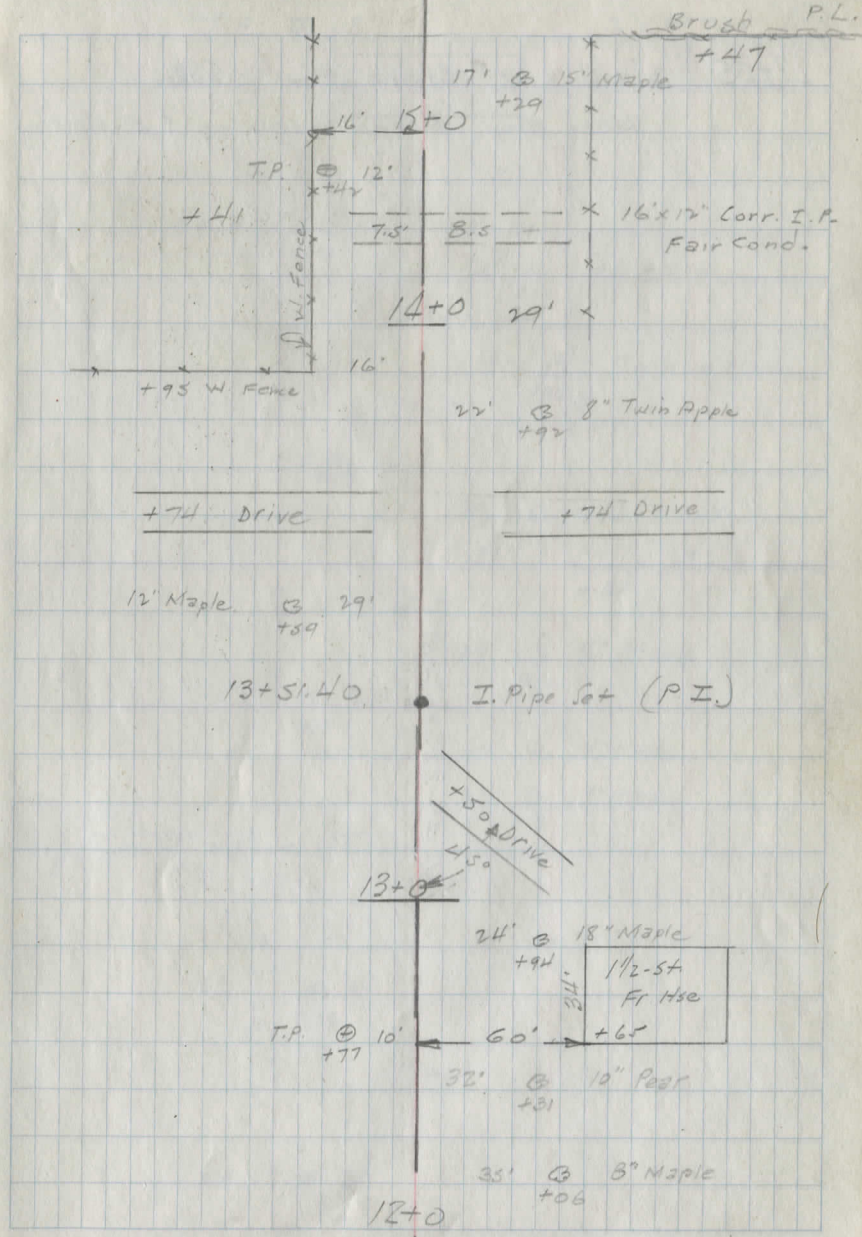
Sta 13+51.40 P.I. $\Delta = 2^{\circ}07'30''$ - Rt.
 I. Pipe Set

64.00

S. & W
 S.W. Root
 18" Maple

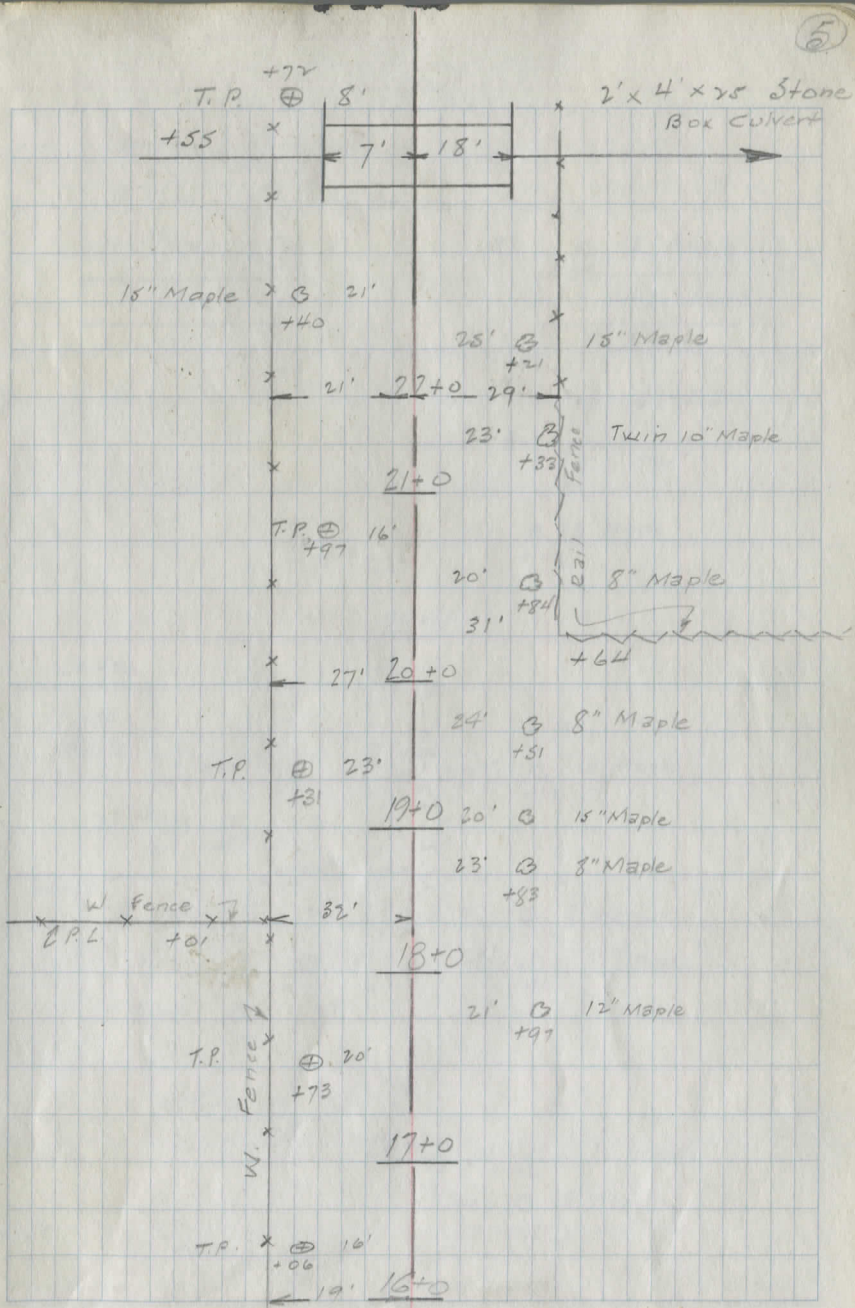
N. 29° 15' E

N. 41° 22' 30" E



22+55 2' x 4' x 25' Stone Box Culvert
 West End Needs repairing & Extending

N. 4° 22' 30" - E



N-41° 22' 30" - E

T.P. ⊕ 18' 26+0

15" Pine ⊖ 29'
+94
18" Pine ⊖ 29'
+79
18" Pine ⊖ 27'
+61

+48 Drive

28' ⊖ 8" Maple
+69

+48 Drive

28' ⊖ 10" Maple
+40
SITED

3' +25'

28' ⊖ 8" Maple
+14

+10
6"
25+0

24+76
1/2 St.
Fr. 13e
59'
27" Maple ⊖
+81

+90

30'
19'

24+48

15" Maple ⊖ 26'
+51
T.P. ⊕ 4'
+40
10" Maple ⊖ 27'
+30

27' ⊖ 10" Maple
+99

27' ⊖ 8" Walnut
+52

28' ⊖ 12" Maple
+40

10" Pine ⊖ 23'
+18

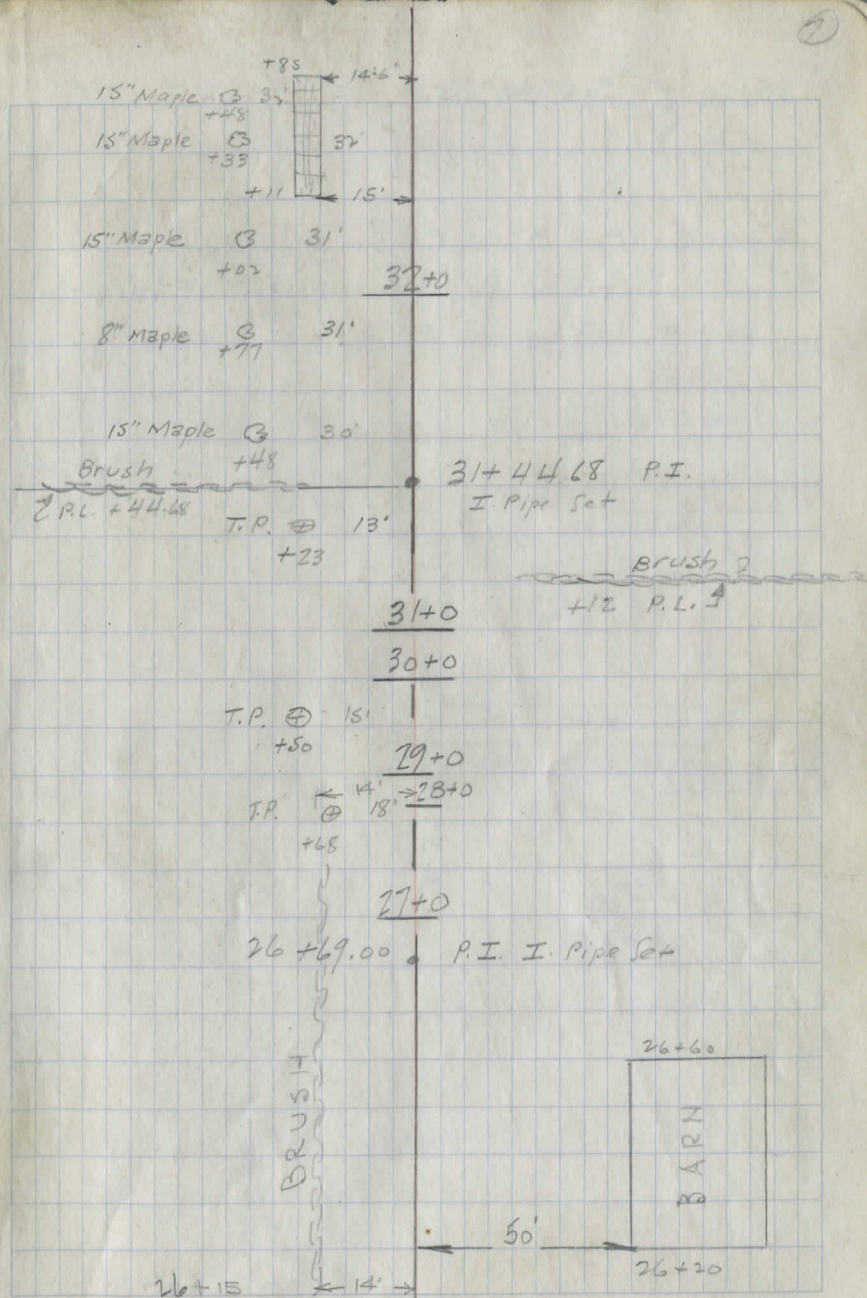
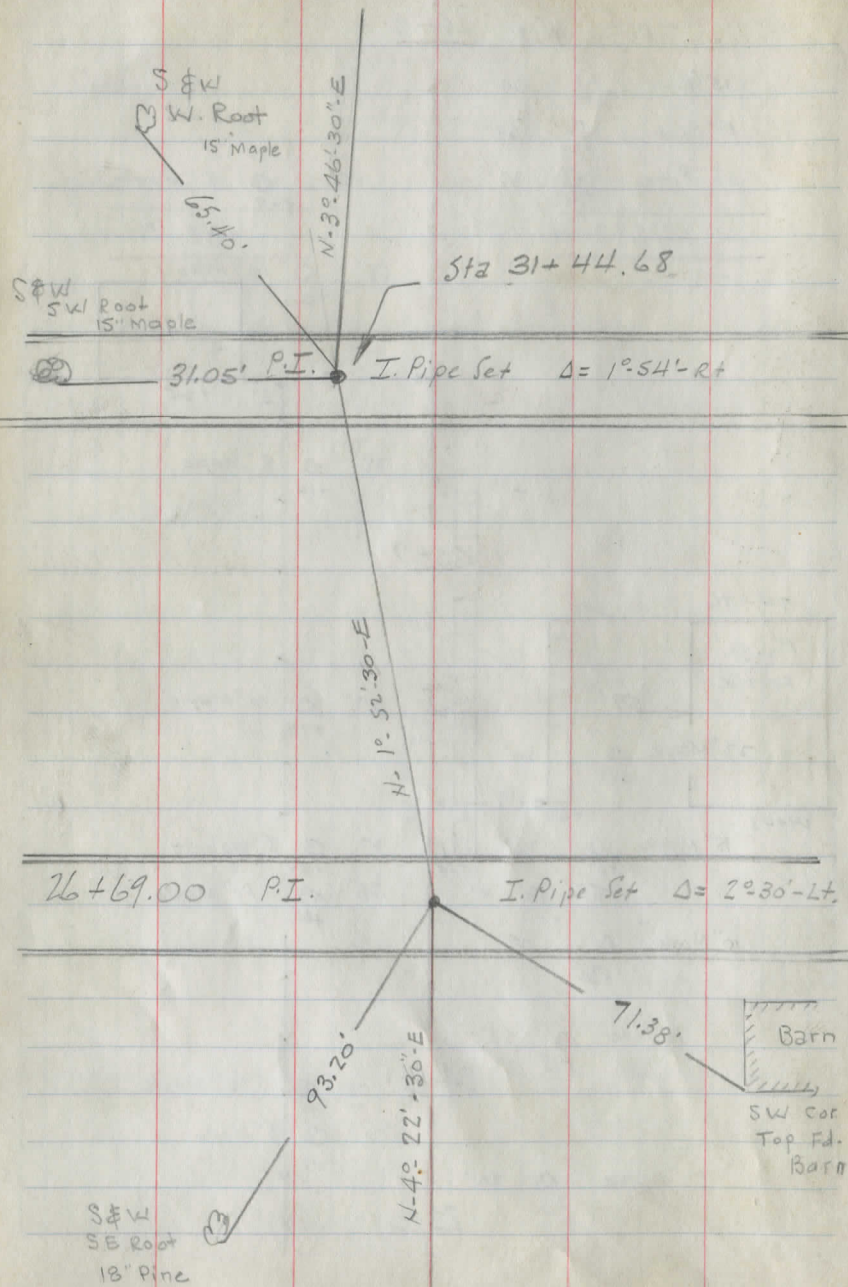
24+0

28' ⊖ 10" Maple
+39

26' ⊖ 8" Maple
+41

12" Apple ⊖ 22'
+06

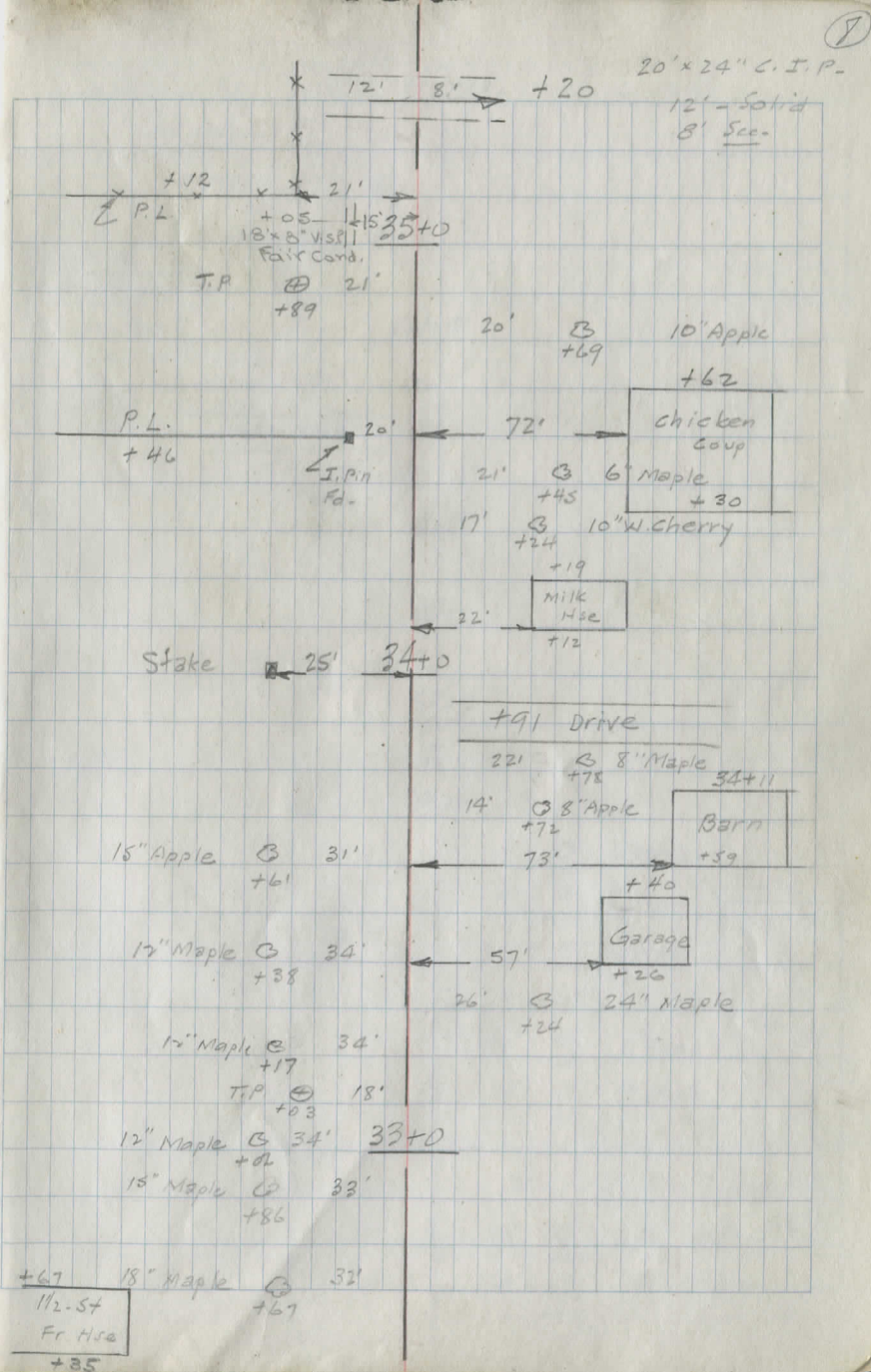
23+0



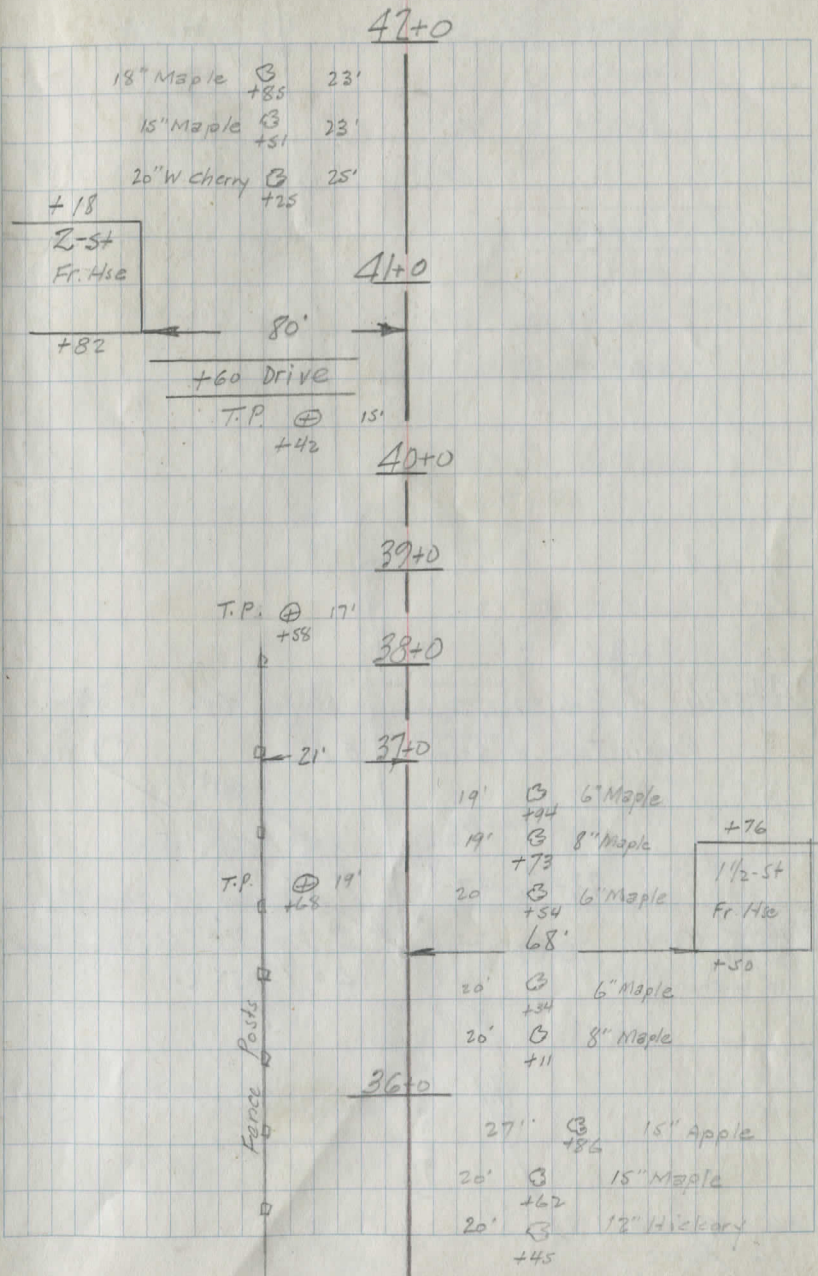
35+20 $\frac{1}{2}$ 20' x 24" C.I.P. Good Cond.

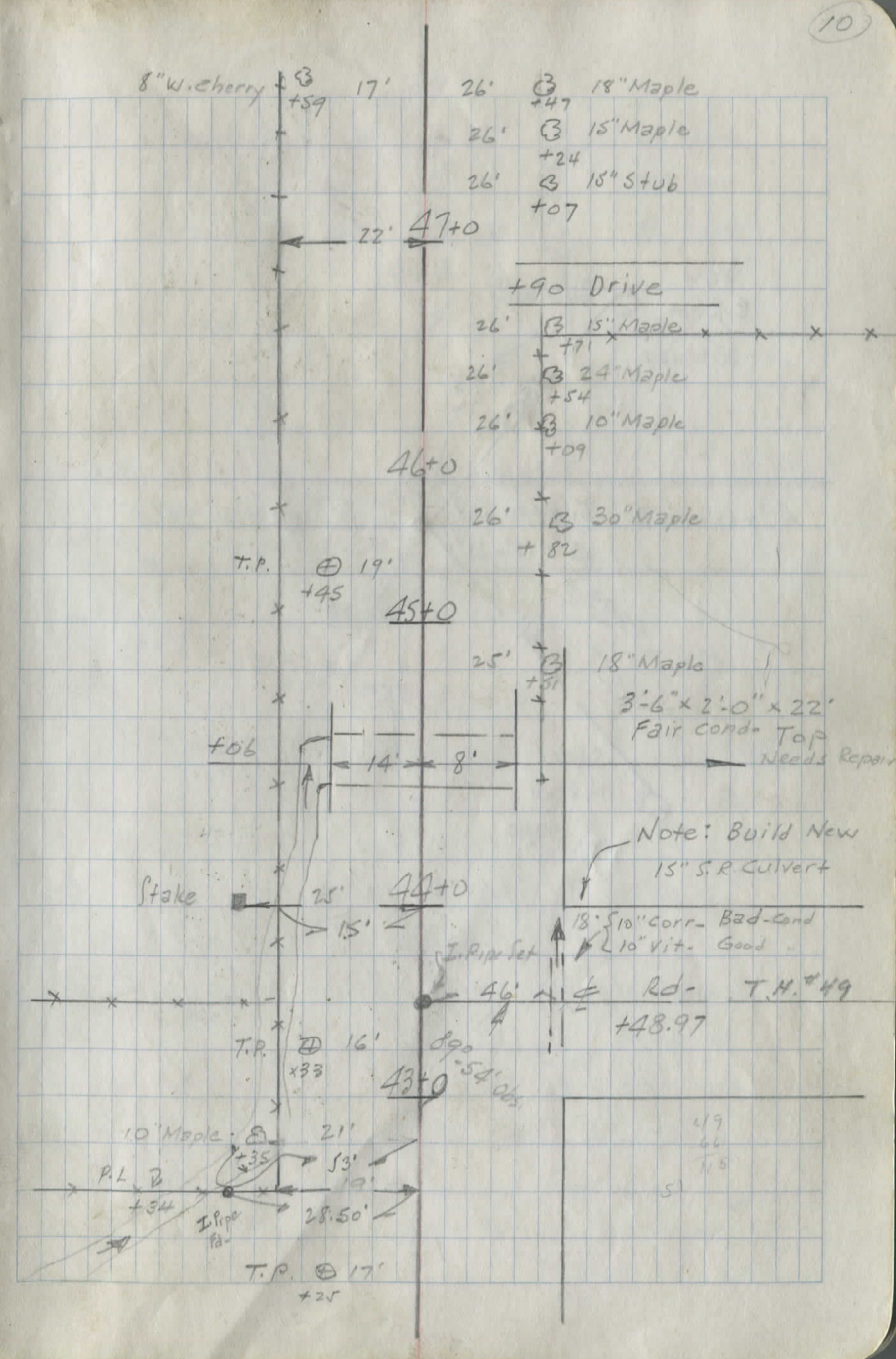
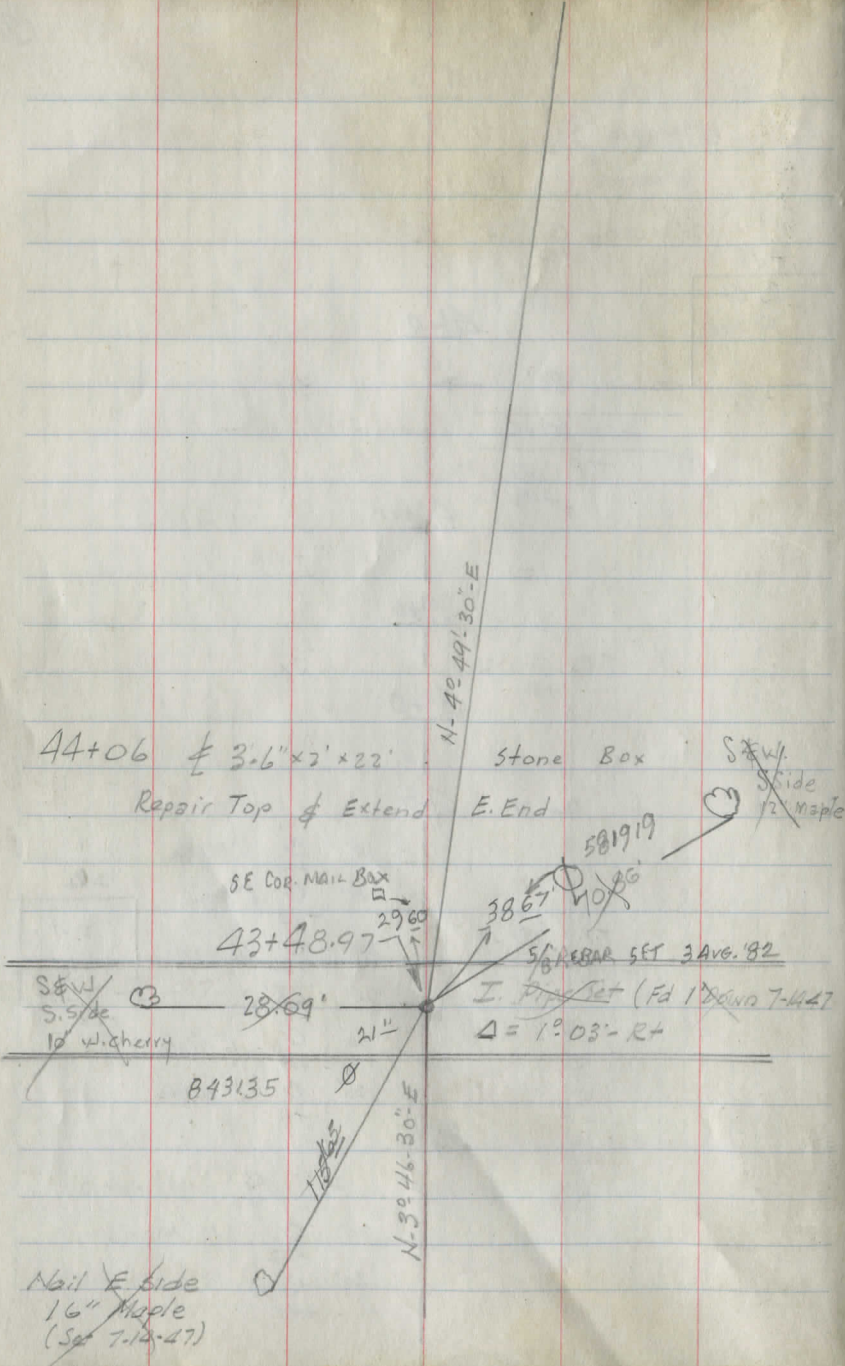
35+05 18' x 8" U.S.P. in Driveway
to be replaced with a larger
Pipe or Eliminated entirely

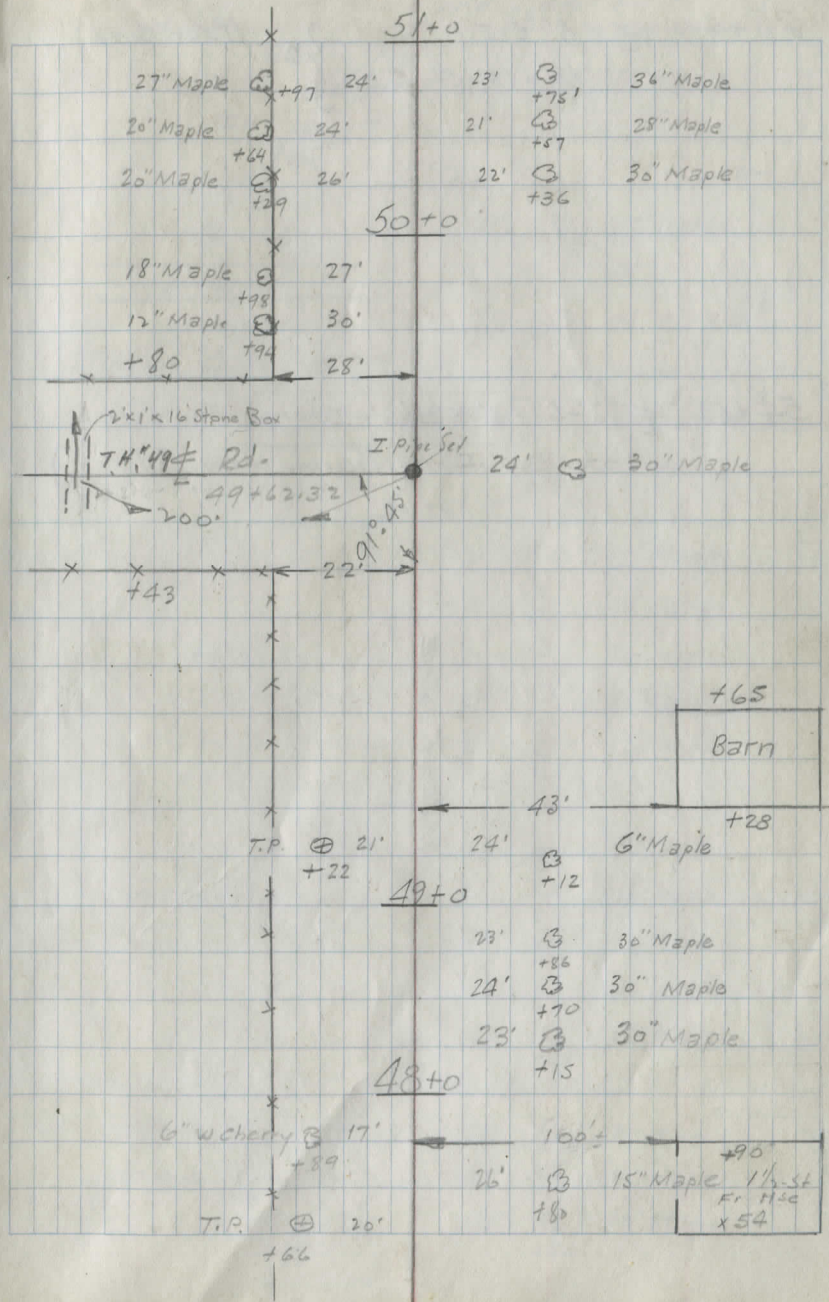
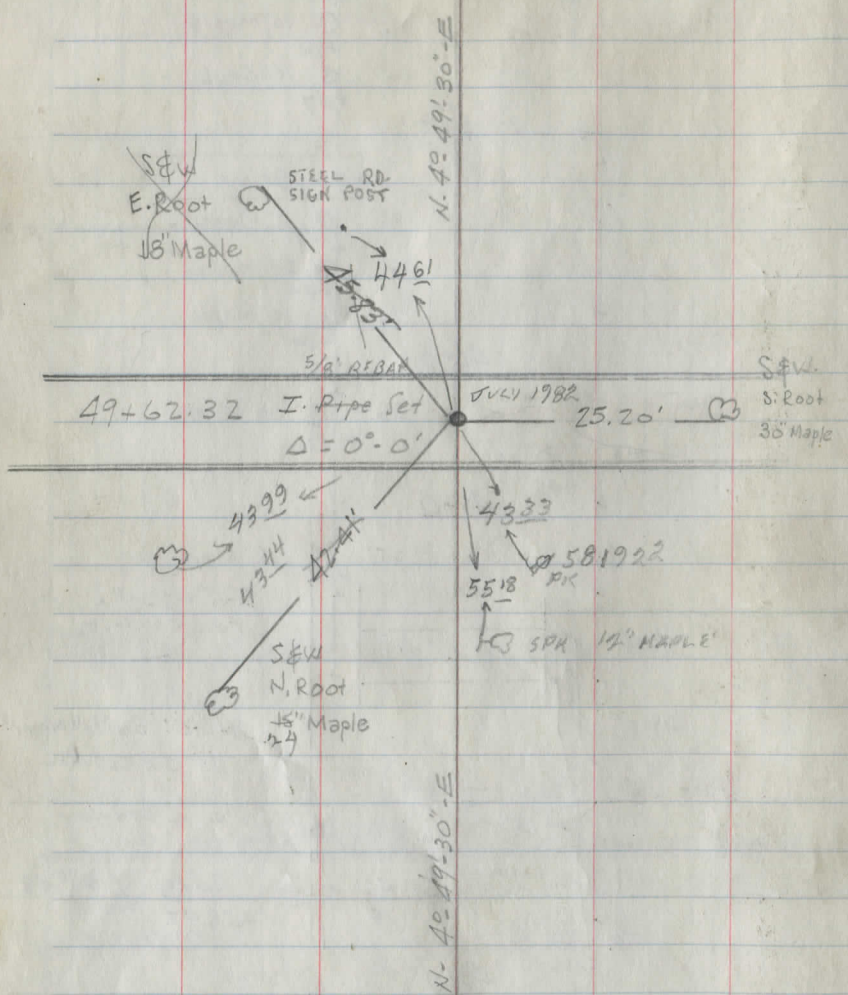
N-30°46'-30"-E



N. 3° 46' 30" E



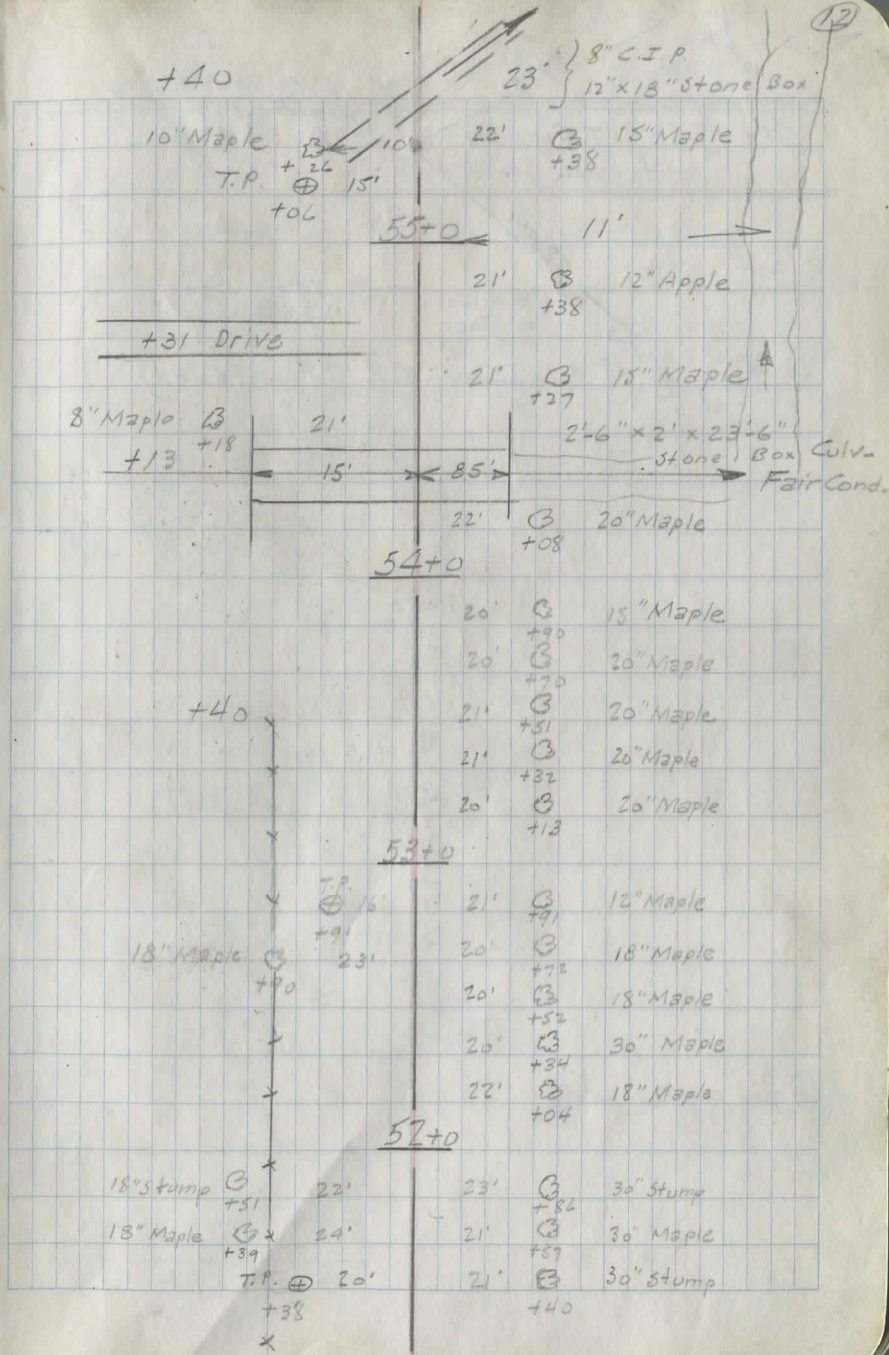




55+40 ∇ 8" C.I.P.
 12" x 18" Stone Box } 23' (Poor Cond.)

54+13 ∇ 2'-6" x 2' x 23'-6" Stone Box Culvert
 (Build New Culvert.)

N. 42° 49' 30" - E



S.W. Root 15" Maple
 Spt 10 0317 03A
 17.3" MAPLE
 6044
 581928
 $\Delta = 0^{\circ} - 0' - 0''$

61+17.50 I. Pipe Set
 5/8 REBAR Sur. 82

32.52'
 36.53'
 S.W. N. Root 15" Maple
 S.W. 11.3 HICKORY

60+61 \pm 18" x 18" Corr I.P. (Poor Cond.)

N. 4° 49' 30" E

15" Maple 31'
 +42
 18" Maple 31'
 +20
 61+31

I. Pipe Set
 +17.50

2-St. Fr. Hse
 +91
 15" Maple 30'
 51'

+92 P.L.
 13' 12" Hickory
 10.5' 18" x 18" Corr. I.P. (Poor Cond.)
 7.5'
 +61

T.P. 14
 +45
 60+0

W.F. 7
 P.L.
 +61
 17'

59+0

58+0

T.P. 14
 +52
 Stake 25' 57+0

8" Maple 31'
 +78

12" Maple 31'
 +54

10" Walnut 31'
 +41

18" Maple 45'
 +16

56+10 Stake 25' 56+0

1 1/2-St. Fr. Hse

25' 20" Maple P.L.
 +95
 +95

55+70 75'

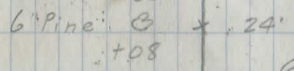
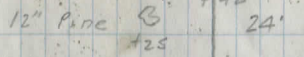
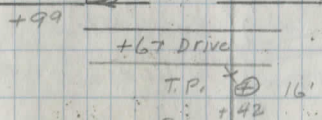
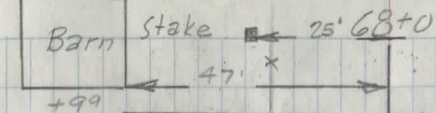
30" Stump 31'
 +70

+62 Drive

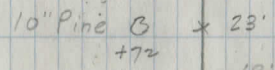
42" Ash 30'

+51

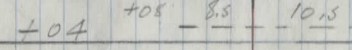
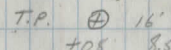
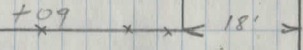
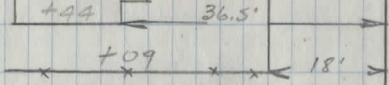
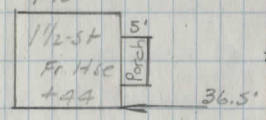
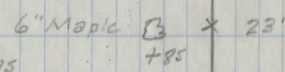
68+26



67+0



18' 66+0

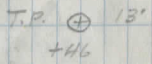


19' x } 15' x 12' Stone Box
 18" Corr. I.P.
 (Poor Cond.)

65+0

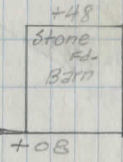
64+0

63+0



36'

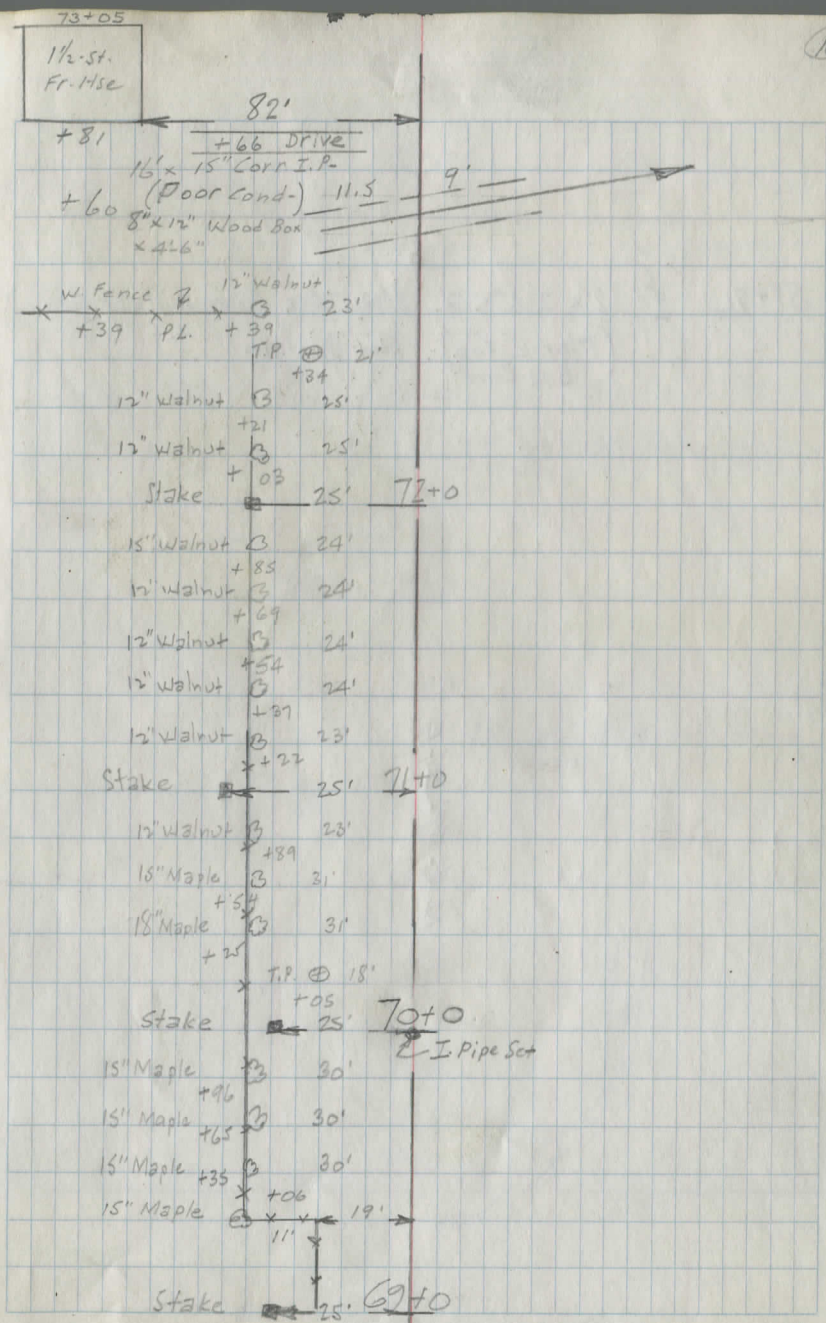
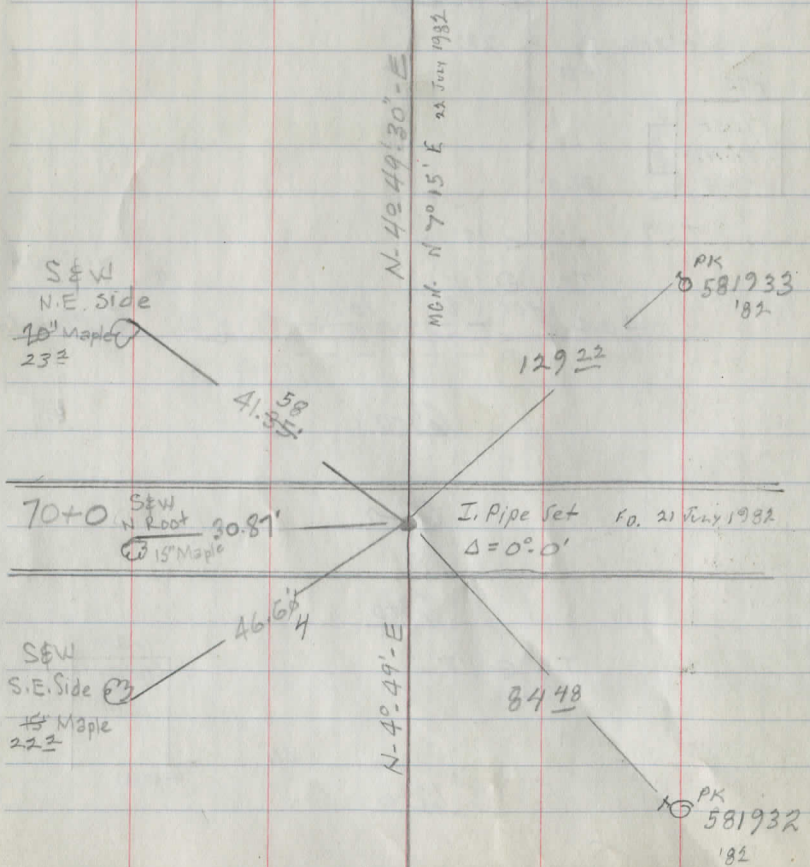
62+0



N-42-49'-30"-E

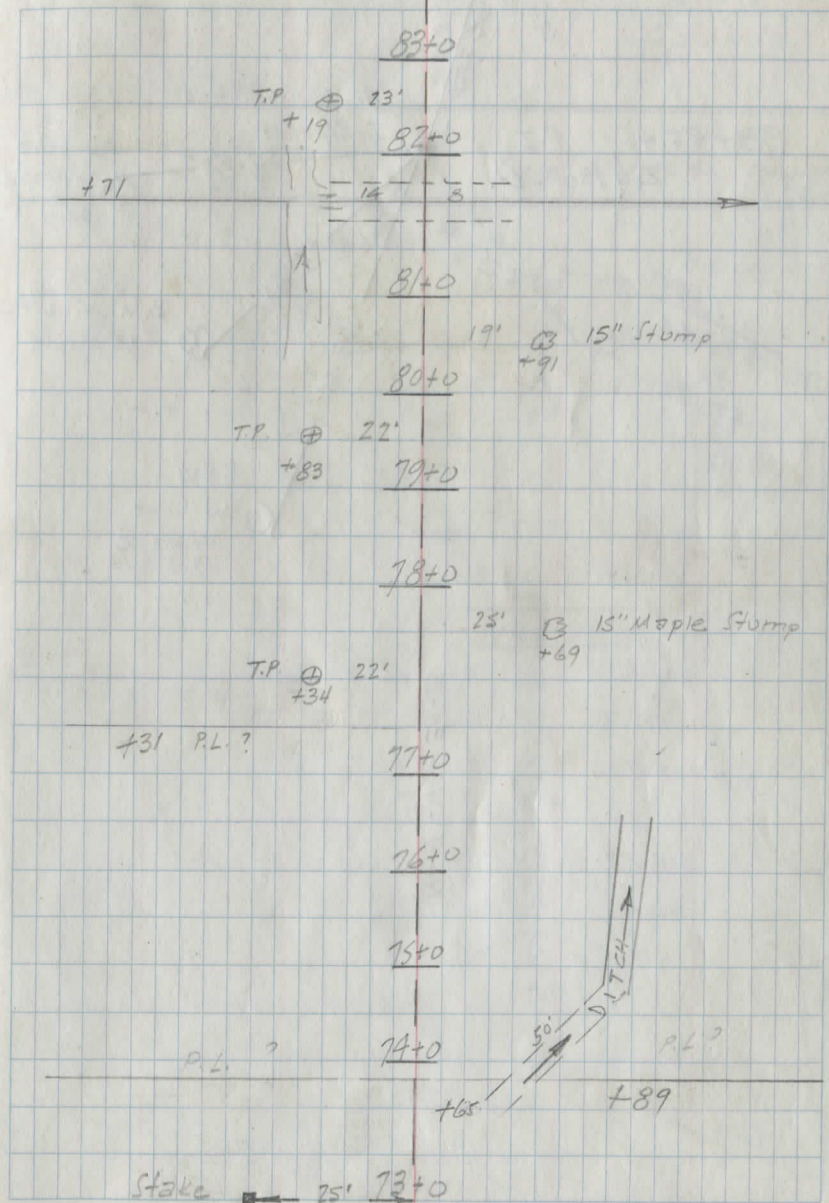
65+04 15" x 12" Stone Box } 19' Poor Cond.
 15" Corr. I.P. } Build New

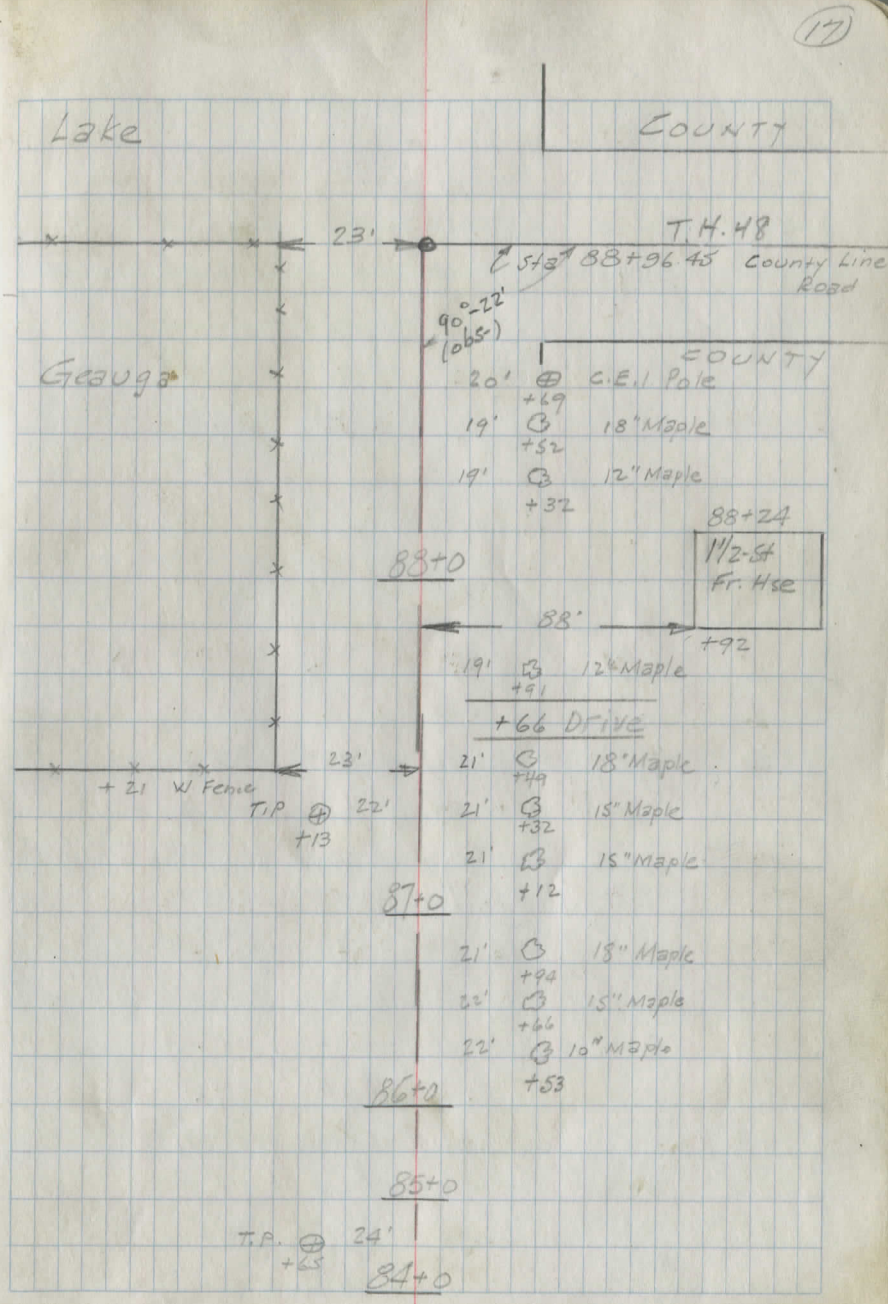
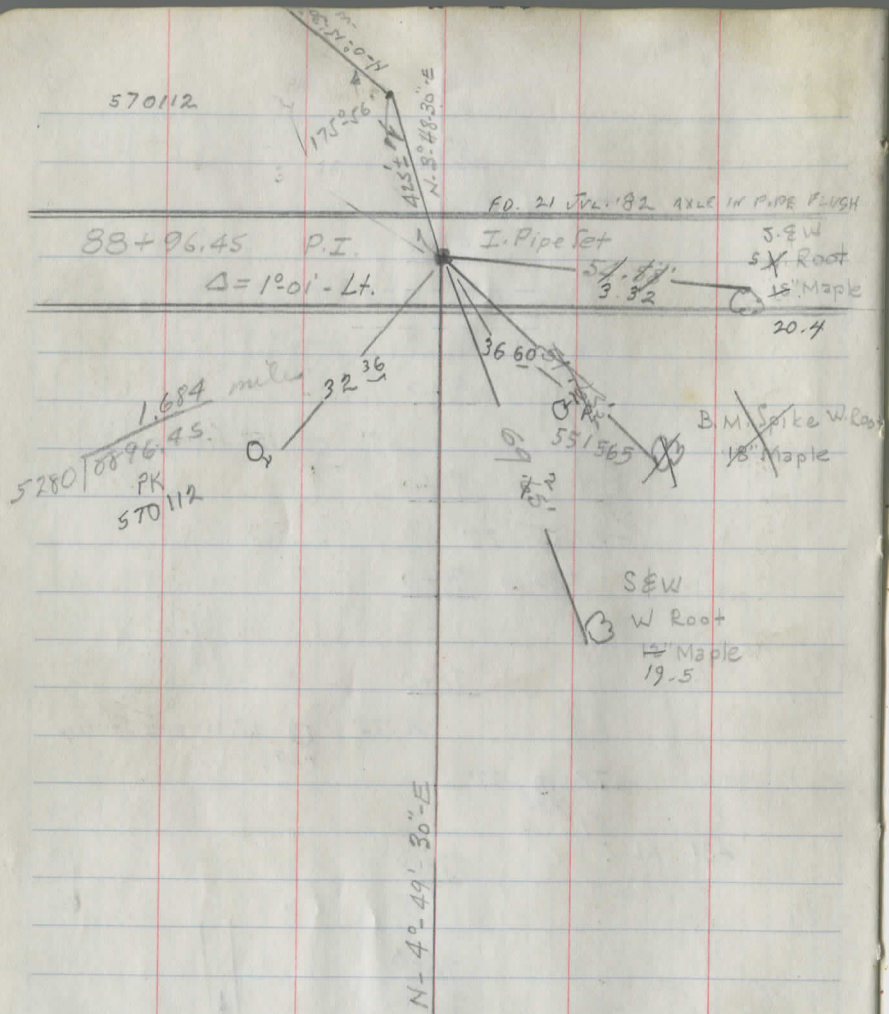
72+60 16' x 15' Corr I.P. } Build New
 8" x 12" x 4'-6" Wood Box } Hillside Culvert



81+71 $\frac{1}{2}$ 2' x 2'-6" x 22' Stone Box Culvert (Fair Cond-)
 (Plank Top) Stone Bottom
 Bad Cond

N. 41° 49' 30" E





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Blank grid page with a blue grid pattern and a vertical red margin line.

CHECK LEVELS

Garris Cor. N. Rd - UNDER ROAD
June 27, 1936 #42

S. Gould Jr.
S. Dietz
E. Richards (19)

	+	H.I.	-	Elev.	Remarks
B.M. (#4)	7.90	1111.67		1103.77	X-6W X
T.P.	11.47	1122.65	0.49	1111.18	N. Hill culvert 100
T.P.	12.55	1134.76	0.44	1122.21	E. of Pass Drive - (ok 15 ft. 28)
T.P.	8.99	1143.75	0.00	1134.76	
T.P.	11.48	1155.02	0.21	1143.54	
T.P.	2.49	1155.93	1.58	1153.44	
				1150.98	Rec # Used
B.M. (#3)			4.92	1151.01	
B.M. #1	5.64	1156.62		1150.98	X-11
T.P.	7.33	1163.40	0.55	1156.07	
T.P.	1.37	1161.21	3.50	1159.84	
T.P.	1.12	1150.09	12.24	1148.97	
B.M. #2			1.75	1148.34	Spike
T.P.	2.81	1141.13	11.77	1138.32	
T.P.	11.62	1151.35	1.40	1139.73	
T.P.	10.27	1161.25	0.34	1151.01	
T.P.	5.44	1165.08	1.64	1159.64	
T.P.	0.24	1157.04	8.28	1156.80	
T.P.	0.51	1145.82	11.73	1145.31	
T.P.	0.48	1133.67	12.63	1133.19	
T.P.	0.84	1123.06	11.45	1122.22	
T.P.	8.10	1128.67	2.49	1120.57	

your B.M. #12

S.W. Cor. N. Hill Wall Culvert Sta 0+0 46' Lt.

in W. Root 12" Maple 34' Rt. Sta 8+16

B.M.	+	H.I.	-	Elev.	Remarks
		1128.67			
B.M.#3			5.43	1123.24	✓ Spike
T.P.	10.67	1139.05	10.29	1128.38	✓
T.P.	1.01	1139.06	1.00	1138.05	✓
T.P.	0.69	1128.16	11.59	1127.47	✓
T.P.	2.30	1118.60	11.86	1116.30	✓
B.M.#4			3.18	1115.42	✓ Spike
T.P.	2.08	1109.22	11.46	1107.14	✓
T.P.	0.36	1098.47	11.11	1098.11	✓
T.P.	2.24	1087.74	12.97	1085.50	✓
B.M.#5			3.12	1084.62	✓ Spike
T.P.	2.59	1081.40	8.93	1078.81	✓
T.P.	0.22	1070.18	11.44	1069.96	✓
T.P.	0.27	1058.95	11.50	1058.68	✓
T.P.	0.83	1049.96	9.82	1049.13	✓
B.M.#6			2.95	1047.01	Spike
T.P.	3.42	1044.83	8.55	1041.41	✓
T.P.	3.65	1041.47	7.01	1037.82	✓
B.M.#7			4.32	1037.15	✓ Spike
T.P.	0.96	1033.74	8.69	1032.78	✓
T.P.	2.10	1029.08	6.76	1026.98	✓
B.M.#8			3.37	1025.71	✓
T.P.	3.15	1024.73	7.50	1021.58	✓
B.M.#9	1.04	1021.14	4.65	1020.08	✓
T.P.	4.58	1020.06	5.64	1015.48	✓

in S.W. Root 8" Maple 26' Rt Sta 23+41

in N.E. Root 12" Maple 34' Lt Sta 33+17

in E. Root 10" Maple 21' Lt. Sta 42+35

in E Root 42" Ash 30' Lt. Sta 55+51

in W Side 6" Maple 23' Lt Sta 65+85 (1' Ab. Gr.)

Spike in N.E. Root 12" Walnut 24' Lt. Sta 71+69

Spike in N.E. Root 15" Maple Stump 25' Rt Sta 77+69

B.M.	+	H.I.	-	Elev.	Rem's
		1020.06	✓		
T.P.	7.82	1024.0	✓	3.86	1016.70 ✓
B.M. #10			3.94	1020.08	Spike

in W. Root 18" Maple 19 Rt. Sta 88+52

Sta	+	H.I.	-	Elev.	Rem's
		1163.73 ✓			
6+0			6.5	1157.2	
7+0			10.2	1153.5	
T.P.	1.25	1155.01 ✓	9.97	1153.76 ✓	
8+0			8.9	1146.1	
				1148.34 ¹⁰⁰	
TP # B.M. #2	0.73	1149.07 ✓	6.67	1148.34 ✓	
9+0			9.6	1139.5	
T.P.	2.73	1141.05 ✓	10.75	1138.32 ✓	
10+0			6.1	1135.0	
+ 43	±	Culvert	7.5	1133.6	
T.P.	7.91	1146.38 ✓	2.88	1138.47 ✓	
11+0			7.8	1138.6	
T.P.	10.76	1156.65 ✓	0.49	1145.89 ✓	
12+0			8.3	1148.4	
T.P.	7.87	1164.16 ✓	0.36	1156.79 ✓	
13+0			6.7	1157.5	
+ 50			4.7	1159.5	
14+0			4.3	1159.9	
+ 41	±	Culvert	4.5	1159.7	

W.	±												E		
	$\frac{4.2}{25'}$	$\frac{6.2}{10'}$	$\frac{6.9}{9'}$	6.5	$\frac{6.5}{2'}$	$\frac{6.9}{9'}$	$\frac{7.4}{11'}$	$\frac{6.4}{13'}$	$\frac{5.6}{25'}$						
	$\frac{3.0}{30'}$	$\frac{3.2}{25'}$	$\frac{3.5}{18'}$	$\frac{7.8}{6'}$	$\frac{10.5}{3'}$	10.2	$\frac{9.9}{8'}$	$\frac{10.5}{16'}$	$\frac{11.3}{18'}$	$\frac{9.8}{20'}$	$\frac{8.3}{22'}$	$\frac{8.8}{30'}$			
					$\frac{2.0}{30'}$	$\frac{1.5}{14'}$	8.9	$\frac{8.0}{3'}$	$\frac{7.6}{12'}$	$\frac{8.3}{19'}$	$\frac{9.0}{23'}$	$\frac{7.0}{25'}$	$\frac{5.5}{27'}$	$\frac{5.8}{32'}$	
	$\frac{0.0}{30'}$	$\frac{1.5}{19'}$	$\frac{3.8}{11'}$	9.6	$\frac{9.8}{4'}$	$\frac{10.4}{5'}$	$\frac{10.4}{16'}$	$\frac{10.9}{25'}$	$\frac{11.0}{27'}$	$\frac{11.7}{29'}$	$\frac{11.1}{31'}$	$\frac{11.7}{36'}$			
					$\frac{9.3}{25'}$	$\frac{8.7}{18'}$	6.1	$\frac{5.2}{6'}$	$\frac{4.8}{14'}$	$\frac{5.3}{23'}$	$\frac{6.4}{25'}$	$\frac{7.9}{33'}$	$\frac{9.2}{40'}$		
	$\frac{10.7}{50'}$	$\frac{11.5}{FL}$	$\frac{7.7}{7HW}$	7.5	$\frac{5.2}{6'}$	$\frac{4.6}{13'}$	$\frac{5.0}{20'}$	$\frac{7.2}{7HW}$	$\frac{12.0}{FL}$	$\frac{15.1}{12'}$					
	$\frac{13.4}{30'}$	$\frac{10.6}{18'}$	$\frac{9.4}{4'}$	$\frac{8.7}{2'}$	7.8	$\frac{7.7}{10'}$	$\frac{8.3}{14'}$	$\frac{8.7}{20'}$	$\frac{8.8}{28'}$	$\frac{9.1}{35'}$					
	$\frac{0.7}{30'}$	$\frac{0.4}{25'}$	$\frac{0.6}{15'}$	$\frac{7.0}{5'}$	$\frac{7.4}{4'}$	$\frac{8.4}{3'}$	8.3	$\frac{8.0}{9'}$	$\frac{8.3}{14'}$	$\frac{8.1}{16'}$	$\frac{7.9}{18'}$	$\frac{1.7}{30'}$	$\frac{0.5}{35'}$		
					$\frac{+0.8}{30'}$	$\frac{+0.6}{25'}$	$\frac{0.9}{14'}$	$\frac{7.3}{4'}$	6.7	$\frac{6.6}{5'}$	$\frac{7.6}{14'}$	$\frac{6.0}{15'}$	$\frac{1.7}{33'}$	$\frac{2.3}{30'}$	$\frac{4.0}{H}$
	$\frac{0.2}{20'}$	$\frac{0.9}{15'}$	$\frac{3.8}{8'}$	$\frac{4.7}{5'}$	4.7	$\frac{4.8}{4'}$	$\frac{5.7}{10'}$	$\frac{4.6}{25'}$							
	$\frac{1.9}{25'}$	$\frac{3.9}{9'}$	$\frac{4.5}{7'}$	4.3	$\frac{4.4}{3'}$	$\frac{4.9}{10'}$	$\frac{4.6}{16'}$	$\frac{5.0}{25'}$							
					$\frac{5.5}{FL}$	4.5	$\frac{5.6}{FL}$	$\frac{9.1}{50'}$							

Sta	+	H.I.	-	Elev.	Remarks
		1144.16 ✓			
15+0			4.2	1160.0	
T.P.	3.37	1163.63 ✓	3.90	1160.26 ✓	
16+0			2.5	1161.1	
			3.5	1160.1	
17+0			5.9	1157.7	
18+0			12.5	1151.1	
T.P.	0.79	1151.89 ✓	12.53	1151.10 ✓	
19+0			9.9	1142.0	
T.P.	0.44	1142.51 ✓	9.82	1142.07 ✓	
20+0			12.2	1130.3	
T.P.	1.42	1134.60 ✓	9.33	1133.15 ✓	Spoke
T.P.	2.70	1124.91 ✓	12.39	1122.21 ✓	in E Root 12" Maple 33' Lt Sta 20+0
21+0			3.0	1121.9	
22+0			6.2	1118.7	
25+0	⊥ Culvert		6.5	1118.4	
T.P.	8.00	1126.20 ✓	6.71	1118.20 ✓	
23+0			6.5	1119.7	
B.M.#3			2.96	1123.24 ✓	
T.P.	10.64	1135.37 ✓	1.47	1124.73 ✓	

W											E	
	1.5	2.8	3.6	4.4	4.2	4.6	5.3	6.5				
	25'	15'	10'	8'		8'	15'	25'				
	1.0	1.5	2.3	3.2	2.9	2.5	3.0	3.3	2.9	3.5		
	25'	15'	11'	10'	7'		8'	10'	11'	25'		
	0.9	1.3	2.7	4.6	4.2	3.5	4.0	4.5	3.3	3.7		
	25'	17'	13'	12'	9'		8'	11'	13'	25'		
	1.2	2.1	6.7	6.2	5.9	6.4	7.3	4.6	4.9			
	25'	19'	12'	8'		8'	11'	15'	25'			
	4.3	4.7	13.2	12.9	12.5	12.9	13.2	8.3	9.3			
	30'	22'	11'	10'		6'	9'	15'	30'			
	1.9	2.4	2.9	10.6	10.1	9.9	10.1	10.7	8.9	4.4	4.1	4.0
	30'	25'	20'	11'	8'		8'	11'	13'	22'	25'	20'
	9.1	9.0	9.2	12.8	12.3	12.2	12.4	13.2	9.1	8.4	8.4	
	30'	25'	18'	13'	8'		10'	14'	20'	25'	30'	
	3.5	3.5	3.4	3.0	2.9	3.4	3.4	3.0	1.8			
	25'	9'	6'			8'	13'	19'	25'			
	8.5	7.4	6.5	6.2	6.1	4.4	6.5	8.2				
	25'	11'	5'		5'	12'	17'	25'				
	13.3	13.0	6.7	6.5	7.0	13.2	13.2	14.6	16.5			
	50'	FL	THW		THW	FL	50'	100'	200'			
	10.6	0.9	6.1	7.0	6.6	6.5	6.1	7.0	8.5	9.0		
	30'	20'	11'	5'	2'		6'	13'	17'	25'		

Sta + H.I. - Elev Rem's

1135.37 ✓

24+0 9.7 1125.7

T.P. 7.34 1141.41 ✓ 1.30 1134.07 ✓

25+0 8.1 1133.3

+48 ± Drives (E & W) ^{6.1} 1125.3

26+0 4.5 1136.9

+50 change in Grade 3.3 1138.1

T.P. 7.47 1138.94 ✓

↳ Interrupted by Rain

(25)

W.

±

E

$\frac{+0.3}{30'}$ $\frac{0.9}{19'}$ $\frac{7.8}{2'}$ 9.7 $\frac{9.4}{2'}$ $\frac{9.1}{8'}$ $\frac{9.6}{15'}$ $\frac{10.2}{17'}$ $\frac{8.3}{20'}$ $\frac{5.9}{25'}$ $\frac{5.1}{30'}$ $\frac{5.5}{35'}$

$\frac{+0.6}{4'}$ $\frac{3.7}{25'}$ $\frac{3.9}{22'}$ $\frac{4.7}{18'}$ $\frac{6.5}{1'}$ 8.1 $\frac{8.5}{1'}$ $\frac{8.0}{41'}$ $\frac{7.8}{10'}$ $\frac{8.3}{15'}$ $\frac{7.7}{20'}$ $\frac{7.2}{25'}$ $\frac{7.5}{30'}$

$\frac{4.7}{30'}$ 6.1 $\frac{7.6}{30'}$

$\frac{0.1}{25'}$ $\frac{1.6}{19'}$ $\frac{5.1}{1'}$ 4.5 $\frac{5.5}{12'}$ $\frac{4.1}{25'}$

8.3 $\left(\frac{2.5}{\text{Barn}}\right)$

Sta	+	H.I.	-	Elev.	Rems
T.P.	1.65	1140.59 ✓		1138.94	
27+0			3.8	1136.8	
28+0			8.2	1132.4	
29+0			12.0	1128.6	
T.P.	0.18	1128.58 ✓	12.19	1128.40 ✓	
30+0			5.2	1123.4	
31+0			9.3	1119.3	
T.P.	1.80	1120.11 ✓	10.27	1118.31 ✓	
32+0			4.2	1115.9	
33+0			9.7	1110.4	
B.M. #4			4.68	1115.43 ✓ 1115.47 read	
T.P.	0.81	1111.81 ✓	9.11	1111.00 ✓	
34+0			4.0	1107.8	
35+0			5.2	1106.6	
+ 20	± Culvert		5.5	1106.3	
36+0			7.8	1104.0	
T.P.	3.00	1106.47 ✓	8.34	1103.47 ✓	
37+0			4.2	1102.3	

W	±												E
	$\frac{+0.3}{25'}$	$\frac{0.0}{22'}$	$\frac{2.4}{14'}$	$\frac{4.5}{10'}$	$\frac{4.0}{7'}$	3.8	$\frac{4.4}{6'}$	$\frac{4.8}{8'}$	$\frac{3.8}{10'}$	$\frac{3.3}{12'}$	$\frac{3.9}{25'}$		
			$\frac{7.5}{25'}$	$\frac{8.3}{11'}$	$\frac{8.8}{10'}$	$\frac{8.3}{7'}$	8.2	$\frac{8.9}{8'}$	$\frac{9.2}{10'}$	$\frac{8.3}{11'}$	$\frac{9.6}{25'}$		
	$\frac{7.9}{25'}$	$\frac{7.9}{23'}$	$\frac{10.7}{7'}$	$\frac{10.4}{13'}$	$\frac{11.3}{11'}$	$\frac{12.5}{9'}$	$\frac{12.0}{8'}$	12.0	$\frac{12.4}{9'}$	$\frac{13.8}{15'}$	$\frac{10.8}{18'}$	$\frac{10.3}{22'}$	$\frac{10.8}{25'}$
	$\frac{1.3}{25'}$	$\frac{1.1}{18'}$	$\frac{4.0}{12'}$	$\frac{3.8}{9'}$	$\frac{5.6}{7'}$	$\frac{5.2}{25'}$	5.2	$\frac{5.2}{3'}$	$\frac{5.7}{11'}$	$\frac{6.4}{14'}$	$\frac{3.7}{19'}$	$\frac{2.5}{25'}$	
			$\frac{5.3}{25'}$	$\frac{5.7}{16'}$	$\frac{10.1}{7'}$	$\frac{9.5}{3'}$	9.3	$\frac{9.3}{2'}$	$\frac{9.9}{13'}$	$\frac{7.1}{16'}$	$\frac{7.6}{25'}$		
			$\frac{0.1}{25'}$	$\frac{1.0}{18'}$	$\frac{4.4}{12'}$	4.2	$\frac{4.7}{10'}$	$\frac{1.9}{14'}$	$\frac{2.4}{25'}$				
	$(\frac{4.4}{25'})$	$\frac{3.9}{25'}$	$\frac{4.0}{23'}$	$\frac{10.0}{12'}$	$\frac{9.5}{3'}$	9.7	$\frac{10.3}{9'}$	$\frac{5.7}{18'}$	$\frac{6.1}{25'}$				
	$\frac{2.0}{25'}$	$\frac{2.0}{21'}$	$\frac{4.2}{16'}$	$\frac{4.5}{11'}$	$\frac{4.2}{7'}$	4.0	$\frac{4.1}{10'}$	$\frac{3.6}{23'}$	$\frac{3.1}{25'}$	$(\frac{2.9}{11.4})$	$(\frac{2.6}{13})$		
	$\frac{6.0}{25'}$	$\frac{5.6}{16'}$	$\frac{6.9}{14'}$	$\frac{5.5}{8'}$	5.2	$\frac{5.5}{7'}$	$\frac{5.2}{11'}$	$\frac{6.4}{25'}$					
			$\frac{7.7}{25'}$	$\frac{5.6}{25'}$	5.5	$\frac{5.8}{25'}$	$\frac{8.1}{25'}$	$\frac{9.8}{25'}$	$\frac{13.4}{200'}$				
	$\frac{6.4}{25'}$	$\frac{7.1}{23'}$	$\frac{1.8}{14'}$	$\frac{8.3}{13'}$	$\frac{7.9}{8'}$	7.8	$\frac{8.0}{8'}$	$\frac{7.4}{10'}$	$\frac{7.3}{25'}$				
	$\frac{2.3}{25'}$	$\frac{2.3}{21'}$	$\frac{4.3}{15'}$	$\frac{4.5}{9'}$	$\frac{4.5}{1'}$	4.2	$\frac{4.7}{7'}$	$\frac{2.9}{13'}$	$\frac{3.8}{25'}$	$(\frac{2.4}{11})$			

Sta	+	H.I.	-	Elev.	Remis
		1106.47			
38+0			7.1	1099.4	
39+0			9.7	1096.8	
T.P.	0.09	1096.09 ✓	10.47 ✓	1096.00 ✓	
40+0			4.0	1092.1	
+60	±	Drive West	6.2	1089.9	
41+0			8.1	1088.0	
42+0			11.7	1084.4	
T.P.	388	1087.70 ✓	12.27	1083.82 ✓	
B.M. #5			3.08	1084.62 ✓	
43+0			6.2	1081.5	
+48 ⁹²	±	Rd. East	7.2	1080.5	
44+0			7.7	1080.0	
+06	±	Culvert	7.9	1079.8	
T.P.	5.33	1084.21 ✓	8.8 ✓	1078.88 ✓	
45+0			5.3	1078.9	
+50			4.8	1079.4	

W	±										E
	$\frac{5.2}{25'}$	$\frac{5.2}{22'}$	$\frac{7.9}{12'}$	$\frac{7.2}{6'}$	7.1	$\frac{7.5}{6'}$	$\frac{7.9}{9'}$	$\frac{7.4}{10'}$	$\frac{6.3}{14'}$	$\frac{6.1}{28'}$	
	$\frac{8.8}{25'}$	$\frac{8.8}{16'}$	$\frac{9.5}{11'}$	$\frac{10.7}{10'}$	$\frac{9.9}{8'}$	9.7	$\frac{10.1}{8'}$	$\frac{10.4}{11'}$	$\frac{9.8}{13'}$	$\frac{9.1}{25'}$	
	$\frac{2.1}{25'}$	$\frac{2.3}{15'}$	$\frac{4.5}{9'}$	$\frac{4.2}{4'}$	4.0	$\frac{3.9}{1'}$	$\frac{4.6}{9'}$	$\frac{5.2}{12'}$	$\frac{3.3}{15'}$	$\frac{3.1}{28'}$	
	$\frac{8.5}{14'}$					$\frac{4.6}{25'}$					
	$\frac{5.8}{25'}$	$\frac{6.5}{16'}$	$\frac{7.8}{11'}$	$\frac{8.4}{10'}$	$\frac{8.1}{7'}$	8.1	$\frac{8.6}{9'}$	$\frac{9.1}{13'}$	$\frac{6.8}{17'}$	$\frac{6.8}{25'}$	
	$\frac{9.9}{25'}$	$\frac{9.4}{18'}$	$\frac{10.4}{16'}$	$\frac{10.8}{11'}$	$\frac{12.1}{9'}$	$\frac{11.9}{7'}$	11.7	$\frac{12.2}{11'}$	$\frac{12.6}{13'}$	$\frac{9.7}{18'}$	$\frac{7.5}{25'}$
	$\frac{6.3}{25'}$	$\frac{6.1}{18'}$	$\frac{5.6}{10'}$	$\frac{6.8}{7'}$	$\frac{6.3}{5'}$	6.2	$\frac{6.6}{15'}$	$\frac{7.3}{19'}$	$\frac{6.3}{21'}$	$\frac{5.5}{25'}$	
						7.2	$\frac{6.9}{16'}$	$\frac{8.5}{11'}$	$\frac{9.1}{11'}$	$\frac{7.5}{100'}$	$\frac{9.4}{100'}$
	$\frac{7.8}{25'}$	$\frac{10.6}{18'}$	$\frac{7.6}{8'}$		7.7	$\frac{7.9}{6'}$	$\frac{7.5}{10'}$	$\frac{10.2}{16'}$	$\frac{7.9}{20'}$	$\frac{9.1}{25'}$	
	4.9	$\frac{11.3}{11'}$	$\frac{6.5}{14'}$		7.9	$\frac{6.4}{14'}$	$\frac{10.9}{12'}$	$\frac{11.9}{30'}$	$\frac{13.2}{100'}$	$\frac{15.0}{150'}$	
	$\frac{3.3}{25'}$	$\frac{3.5}{21'}$	$\frac{5.4}{13'}$	$\frac{5.7}{10'}$	5.3	$\frac{5.4}{9'}$	$\frac{5.8}{12'}$	$\frac{4.9}{14'}$	$\frac{5.1}{25'}$		
	$\frac{2.7}{25'}$	$\frac{3.7}{21'}$	$\frac{5.0}{16'}$	$\frac{5.6}{13'}$	$\frac{5.0}{10'}$	4.8	$\frac{5.2}{9'}$	$\frac{5.4}{11'}$	$\frac{4.5}{14'}$	$\frac{4.9}{21'}$	

Sta	+	H.I.	-	Elev.	Rem's
		1084.21 ✓			
46+0			5.6	1078.6	
47+0			8.8	1075.4	
T.P.	1.89	1077.14 ✓	8.96	1075.25 ✓	
48+0			5.1	1072.0	
49+0			8.1	1069.0	
46+31	± Rd West		9.9	1067.7	
T.P.	1.34	1068.54 ✓	9.94	1067.20 ✓	
50+0			8.7	1065.8	
51+0			8.5	1060.0	
52+0			13.0	1055.5	
T.P.	0.91	1056.25 ✓	13.20	1055.34 ✓	
53+0			4.1	1052.7	
54+0			6.8	1049.5	
+13	± Culvert		7.1	1049.2	
T.P.	1.19	1050.68 ✓	6.76	1049.49 ✓	
55+0			3.7	1047.0	
B.M.#6			3.67	1047.07 ✓	

(28)

W											E						
	$\frac{3.3}{25'}$	$\frac{3.8}{18'}$	$\frac{5.4}{15'}$	$\frac{6.7}{12'}$	$\frac{6.0}{10'}$	5.6	$\frac{6.0}{9'}$	$\frac{6.3}{12'}$	$\frac{5.1}{14'}$	$\frac{5.4}{25'}$							
	$\frac{6.0}{25'}$	$\frac{6.0}{23'}$	$\frac{9.2}{13'}$	$\frac{8.8}{10'}$	8.8	$\frac{9.1}{8'}$	$\frac{8.1}{25'}$										
	$\frac{1.6}{25'}$	$\frac{2.5}{18'}$	$\frac{5.8}{13'}$	$\frac{5.2}{11'}$	5.1	$\frac{5.4}{7'}$	$\frac{5.8}{10'}$	$\frac{3.5}{15'}$	$\frac{4.0}{25'}$	($\frac{7.8}{11'}$)							
	$\frac{5.3}{25'}$	$\frac{6.5}{19'}$	$\frac{9.2}{12'}$	$\frac{8.4}{8'}$	8.1	$\frac{8.5}{8'}$	$\frac{8.8}{10'}$	$\frac{8.3}{11'}$	$\frac{6.6}{25'}$								
										($\frac{0.5}{B}$)							
						$\frac{17.1}{100'}$	$\frac{10.0}{30'}$	9.9									
						$\frac{1.6}{25'}$	$\frac{2.5}{18'}$	$\frac{3.7}{15'}$	2.7	$\frac{3.4}{9'}$	$\frac{2.5}{12'}$	$\frac{1.4}{25'}$					
						$\frac{5.9}{25'}$	$\frac{5.7}{22'}$	$\frac{9.1}{12'}$	$\frac{8.7}{9'}$	8.5	$\frac{8.7}{12'}$	$\frac{5.7}{21'}$	$\frac{5.7}{25'}$				
						$\frac{10.5}{25'}$	$\frac{10.5}{19'}$	$\frac{13.4}{10'}$	$\frac{13.1}{6'}$	13.0	$\frac{13.5}{9'}$	$\frac{10.4}{16'}$	$\frac{9.9}{25'}$				
						$\frac{4.4}{25'}$	$\frac{4.0}{17'}$	$\frac{4.5}{12'}$	$\frac{4.4}{8'}$	4.1	$\frac{4.7}{11'}$	$\frac{1.6}{18'}$	$\frac{1.6}{25'}$				
						$\frac{8.1}{30'}$	$\frac{8.4}{25'}$	$\frac{9.7}{21'}$	$\frac{7.2}{9'}$	6.8	$\frac{7.1}{6'}$	$\frac{9.5}{12'}$	$\frac{7.8}{11'}$	$\frac{6.8}{25'}$			
						$\frac{8.6}{50'}$	$\frac{11.3}{FL}$	$\frac{6.7}{T_{low}}$	7.1	$\frac{6.7}{T_{low}}$	$\frac{11.2}{FL}$						
						$\frac{5.1}{25'}$	$\frac{5.3}{20'}$	$\frac{4.6}{15'}$	$\frac{4.0}{8'}$	3.7	$\frac{3.8}{9'}$	$\frac{6.4}{12'}$	$\frac{6.6}{15'}$	$\frac{4.1}{19'}$	$\frac{3.3}{22'}$	$\frac{4.6}{25'}$	$\frac{5.1}{30'}$

Sta	+	H.I.	-	Elev	Remarks
65+0		1040.86 ✓	4.5	1036.4	
66+0	} ± Culvert B.M. #7 } outlet in Rd Ditch		4.5	1036.4	
			3.70	1037.15 rcc 1037.16 ✓	
66+0			6.1	1034.8	
67+0			8.3	1034.6	
68+0			10.7	1030.7	
T.P.	2.99	1034.99 ✓	10.86	1030.00 ✓	
69+0			4.4	1028.6	
70+0			5.6	1027.4	
71+0	} 71+25 to 72+5 B.M. #8 } Rock Exposed in Rd Bed		6.8	1026.7	
			7.29	1025.70 ✓	
72+0			9.2	1023.8	
T.P.	3.35	1027.00 ✓	9.34	1023.65 ✓	
76+0	} ± Culvert		3.8	1023.7	
73+0			4.5	1022.5	
76.5			5.7	1021.8	Outlet Ditch (NE)

W											E
	4.1	4.0	5.4	5.1	4.3	4.5	4.8	5.7	4.7	5.2	
	25'	12'	11'	8'	5'		9'	12'	14'	25'	
		4.8	6.2			4.5	6.1				
		30'	FL.				FL.				
(4.0)	4.9	4.8	5.9	7.0	6.6	6.1	6.4	7.0	7.0	5.4	5.3
H	25'	19'	13'	11'	7'		6'	11'	13'	19'	25'
	6.4	6.7	8.0	9.0	8.8	8.3	8.9	10.0	8.0	7.0	6.7
	25'	20'	15'	14'	11'		6'	9'	13'	25'	30'
	9.2	9.3	11.1	10.8		10.7	11.2	12.0	9.7	9.1	9.2
	25'	17'	14'	9'			6'	9'	15'	25'	30'
	1.5	2.3	5.2	4.7	4.3	4.4	4.8	5.4	3.7	3.7	
	25'	16'	12'	11'	7'		7'	9'	11'	25'	
	3.7	4.0	6.5	5.8	5.5	5.6	6.2	6.8	5.3	4.9	
	25'	16'	14'	12'	7'		5'	9'	11'	25'	
	6.3	6.6	7.8	6.9	6.7	6.8	7.3	8.2	7.3	6.6	
	25'	15'	13'	10'	7'		6'	8'	12'	25'	
	9.9	8.9	9.2	9.7	8.9	9.2	9.6	9.8	8.8	8.8	
	25'	13'	14'	17'	10'		7'	11'	19'	25'	
					3.5	5.1	3.8	5.6			
					30'	FL.		FL.			
(0.3)	3.6	4.0	5.7	5.4	4.6	4.5	4.8	5.7	5.5	4.5	4.9
H	25'	20'	16'	13'	11'		6'	8'	11'	13'	25'
						5.7	6.8	8.0	8.7		
							FL.	50'	150'		

Sta	H I	Elev	Remarks
74+0	1027.00 ✓	5.4	1021.6
75+0		5.5	1021.5
T.P.	2.45 1023.25 ✓	6.20	1020.80 ✓
76+0		3.2	1020.1
77+0		4.2	1019.1
B.M. #9		3.14	1020.11 ✓
+40	Ditch West	4.8	1018.5
78+0		5.0	1018.3
79+0		6.7	1016.6
80+0		7.5	1015.8
T.P.	4.01 1019.61 ✓	7.65	1015.60 ✓
81+0		4.0	1015.6
+71	♠ culvert	4.1	1015.5
82+0		4.3	1015.3
83+0		4.6	1015.0

W	E
$\frac{4.2}{25}$	$\frac{5.8}{25}$
$\frac{4.7}{20}$	$\frac{6.2}{19}$
$\frac{6.4}{10}$	$\frac{7.3}{17}$
$\frac{6.1}{14}$	$\frac{6.5}{15}$
$\frac{5.6}{13}$	$\frac{5.7}{20}$
$\frac{5.6}{11}$	5.4
5.4	$\frac{5.8}{9}$
$\frac{6.1}{9}$	$\frac{5.2}{13}$
$\frac{5.2}{13}$	$\frac{5.8}{25}$
$\frac{5.8}{25}$	$\frac{6.2}{19}$
$\frac{6.2}{19}$	$\frac{7.3}{17}$
$\frac{7.3}{17}$	$\frac{6.5}{15}$
$\frac{6.5}{15}$	$\frac{5.7}{20}$
5.5	5.5
$\frac{5.8}{9}$	$\frac{6.7}{10}$
$\frac{6.7}{10}$	$\frac{7.3}{12}$
$\frac{7.3}{12}$	$\frac{6.1}{14}$
$\frac{6.1}{14}$	$\frac{6.7}{25}$
$\frac{1.6}{25}$	$\frac{3.0}{19}$
$\frac{3.0}{19}$	$\frac{4.5}{16}$
$\frac{4.5}{16}$	$\frac{3.6}{10}$
$\frac{3.6}{10}$	3.2
3.2	$\frac{3.9}{9}$
$\frac{3.9}{9}$	$\frac{4.8}{12}$
$\frac{4.8}{12}$	$\frac{3.5}{13}$
$\frac{3.5}{13}$	$\frac{4.0}{25}$
$\frac{2.5}{25}$	$\frac{3.5}{19}$
$\frac{3.5}{19}$	$\frac{5.8}{15}$
$\frac{5.8}{15}$	$\frac{5.0}{11}$
$\frac{5.0}{11}$	4.2
4.2	$\frac{5.0}{8}$
$\frac{5.0}{8}$	$\frac{5.8}{11}$
$\frac{5.8}{11}$	$\frac{5.8}{12}$
$\frac{5.8}{12}$	$\frac{3.8}{16}$
$\frac{3.8}{16}$	$\frac{4.1}{25}$
$\frac{3.1}{30}$	$\frac{6.4}{FL}$
4.8	8.2
8.2	135.0
← Main Outlet Channel (N.E)	
$\frac{3.6}{25}$	$\frac{3.6}{20}$
$\frac{7.0}{15}$	$\frac{6.2}{14}$
$\frac{6.2}{14}$	$\frac{5.3}{10}$
5.0	5.9
5.9	$\frac{6.7}{12}$
$\frac{6.7}{12}$	$\frac{4.9}{15}$
$\frac{4.9}{15}$	$\frac{4.5}{25}$
$\frac{4.3}{25}$	$\frac{4.6}{20}$
$\frac{7.7}{15}$	$\frac{2.5}{14}$
$\frac{6.6}{10}$	6.7
6.7	$\frac{7.6}{10}$
$\frac{6.0}{14}$	$\frac{5.2}{21}$
$\frac{5.2}{21}$	$\frac{6.0}{25}$
$\frac{5.7}{25}$	$\frac{6.7}{20}$
$\frac{8.6}{14}$	$\frac{7.9}{10}$
7.5	$\frac{8.2}{12}$
$\frac{7.1}{14}$	$\frac{6.4}{25}$
$\frac{3.3}{25}$	$\frac{4.7}{18}$
$\frac{5.9}{15}$	$\frac{5.6}{14}$
$\frac{4.3}{11}$	4.0
4.0	$\frac{4.7}{10}$
$\frac{5.2}{13}$	$\frac{3.8}{15}$
$\frac{3.0}{25}$	
7.0	$\frac{4.3}{FL}$
4.1	$\frac{4.5}{THW}$
$\frac{7.2}{FL}$	$\frac{8.3}{100}$
$\frac{9.4}{200}$	
$\frac{3.3}{25}$	$\frac{4.5}{19}$
$\frac{6.8}{16}$	$\frac{4.8}{12}$
4.3	$\frac{4.7}{11}$
$\frac{5.8}{11}$	$\frac{4.4}{13}$
$\frac{5.2}{25}$	
$\frac{3.3}{25}$	$\frac{4.1}{19}$
$\frac{5.0}{18}$	$\frac{5.3}{16}$
4.6	$\frac{5.3}{12}$
$\frac{3.9}{15}$	$\frac{4.0}{25}$

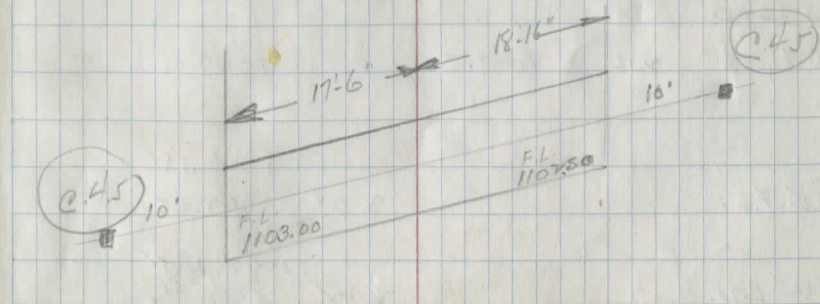
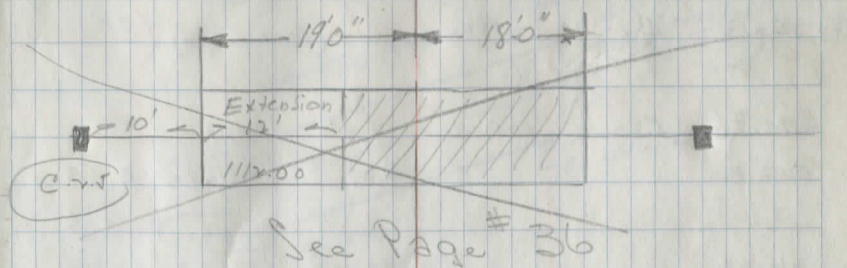
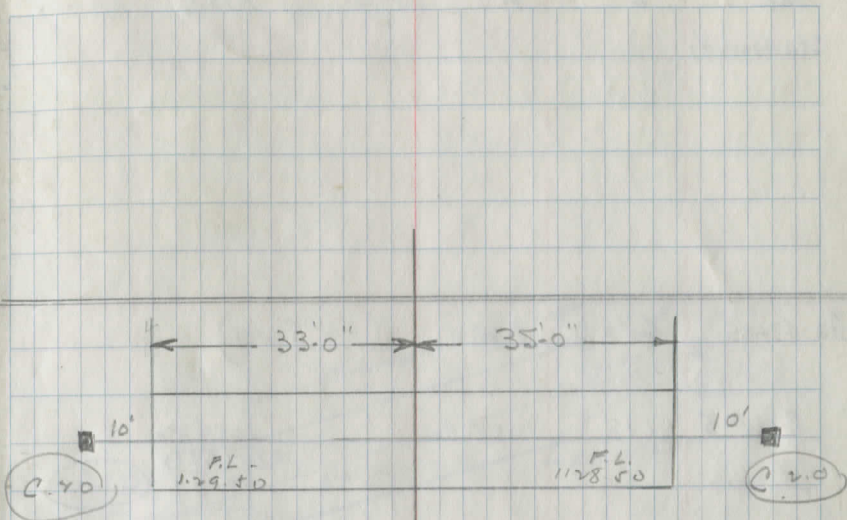
Sta	+	H.I.	-	Elev.	Remarks
84+0		1019.61 ✓	4.0	1015.6	
T.P.	5.27	1021.19 ✓	3.69	1015.94 ✓	
85+0			4.7	1016.5	
86+0			4.8	1016.4	
87+0			4.0	1017.2	
T.P.	5.53	1022.85 ✓	2.87	1018.32 ✓	
+65			4.4	1019.5	
88+0			5.2	1018.7	
+96.45	1/2	County Line Rd.	5.3	1018.6	
89+0			5.3	1018.6	
90+0			5.4	1018.5	
91+0			5.6	1018.3	
92+0			5.7	1018.4	
BM #10			3.77	1020.08 ✓	

W	E
3.3 25'	4.0 12'
5.3 15'	4.8 14'
4.8 13'	3.5 14'
	3.7 25'
4.2 25'	4.7 12'
5.7 17'	4.6 15'
6.7 14'	4.9 25'
5.1 6'	
4.1 25'	4.8 9'
4.7 18'	5.3 12'
5.5 14'	4.8 12'
5.0 8'	5.4 25'
4.4 25'	4.0 5'
4.8 14'	4.2 6'
3.9 12'	4.0 6'
3.6 3'	4.0 25'
3.7 25'	4.4 25'
3.2 23'	2.9 25'
4.8 18'	
6.5 16'	
4.8 14'	
3.5 25'	5.2 2'
4.0 20'	4.8 4'
6.4 16'	4.2 25'
5.0 13'	4.6 14'
4.7 8'	
4.6 25'	5.3 7'
5.8 17'	4.8 11'
7.0 16'	5.8 25'
5.7 12'	7.4 100'
	9.7 200'
	5.3
	5.4
	5.6
	5.7

CULVERTS-

GARRIS CORNERS N. 20-7/29/32 J. Gould Jr
E.C. Richards

Sta	+	H.I.	-	Elev.	Rem's
0+0					
Sta 10+43					
B.M. #1	0.47	1148.81		1148.34	
T.P.	3.82	1140.80	11.83	1136.98	
				1031.65	(C. 2.0)
W. Hub			9.15	1129.65	(C. 2.0)
E. Hub			10.45	1128.35	(C. 2.0)
Sta 22+55					
B.M. #3	2.40	1125.64		1123.24	
T.P.	4.01	1122.94	6.71	1118.93	
W. Hub-			8.29	1114.65	(C. 2.5)
				1112.15	(C. 2.5)
Sta 35+20					
B.M. #4	0.25	1115.47		1115.42	
				1107.64	
W. Hub			7.83	1103.14'	(C. 4.5)
				1106.86	
E. Hub			8.61	1102.36	(C. 4.5)



Sta + M.I. - Elev. Remarks

Sta 43+48.97

Sta 43+85 40' x 36" R.C.P. (40° Skew)

B.M. #5 1.18 1085.80 1084.67

E. Hub 6.43 1075.37 (C. 4.0)

1076.17 (C. 5.0)

W. Hub 4.68 1081.17

Sta 54+13 4' x 2'-6" x 36" Storm Box (Conc. Top) (35° Skew)

B.M. #6 5.80 1057.81 1047.01

East Hub 4.95 1044.36 (C. 3.5)

1045.14

West Hub 6.17 1046.64 (C. 1.5)

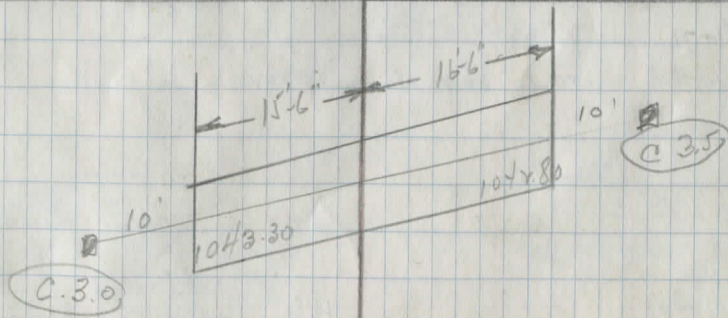
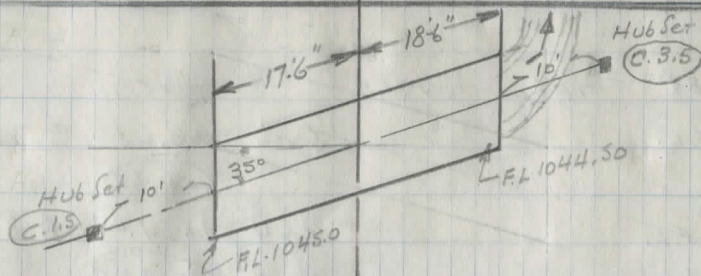
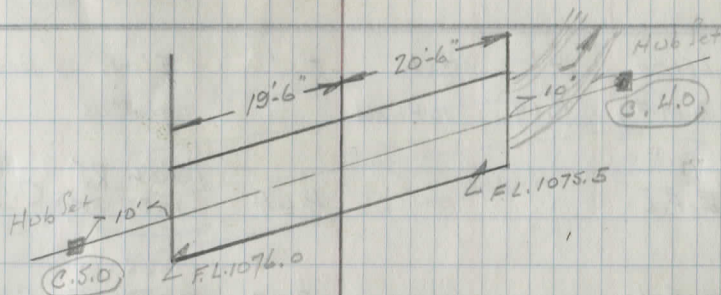
Sta 56+0

B.M. #6 v.l. 1049.17 1047.01

E.F.L. 3.07 1046.15 / 1047.65

W.L.W. 7.77 1046.45 / 1043.45

≠ Rd.



Sta	+	H.I.	-	Elev.	Rem's
60+61		36' x 15' R.C.P.		35° Skew	
B.M. #7	3.82	1040.97			1037.15
T.P.	6.40	1043.60	3.77	1037.20	
E.F.L.			5.94	1036.66	C.1.0
W.F.L.			2.66	1040.94	C.3.5
				1037.44	

Sta	+	H.I.	-	Elev.	Rem's
65+04					
B.M. #7	4.19	1041.34		1037.15	
E.F.L.			4.49	1036.85	C.3.5
				1033.35	
W.F.L.			3.19	1038.15	C.4.0
				1034.15	

Sta	+	H.I.	-	Elev.	Rem's
71+60					
B.M. #8	7.98	1028.69		1025.71	
E.F.L.			5.04	1023.65	C.3.0
				1020.65	
W.F.L.			4.24	1024.45	C.3.0
				1021.45	

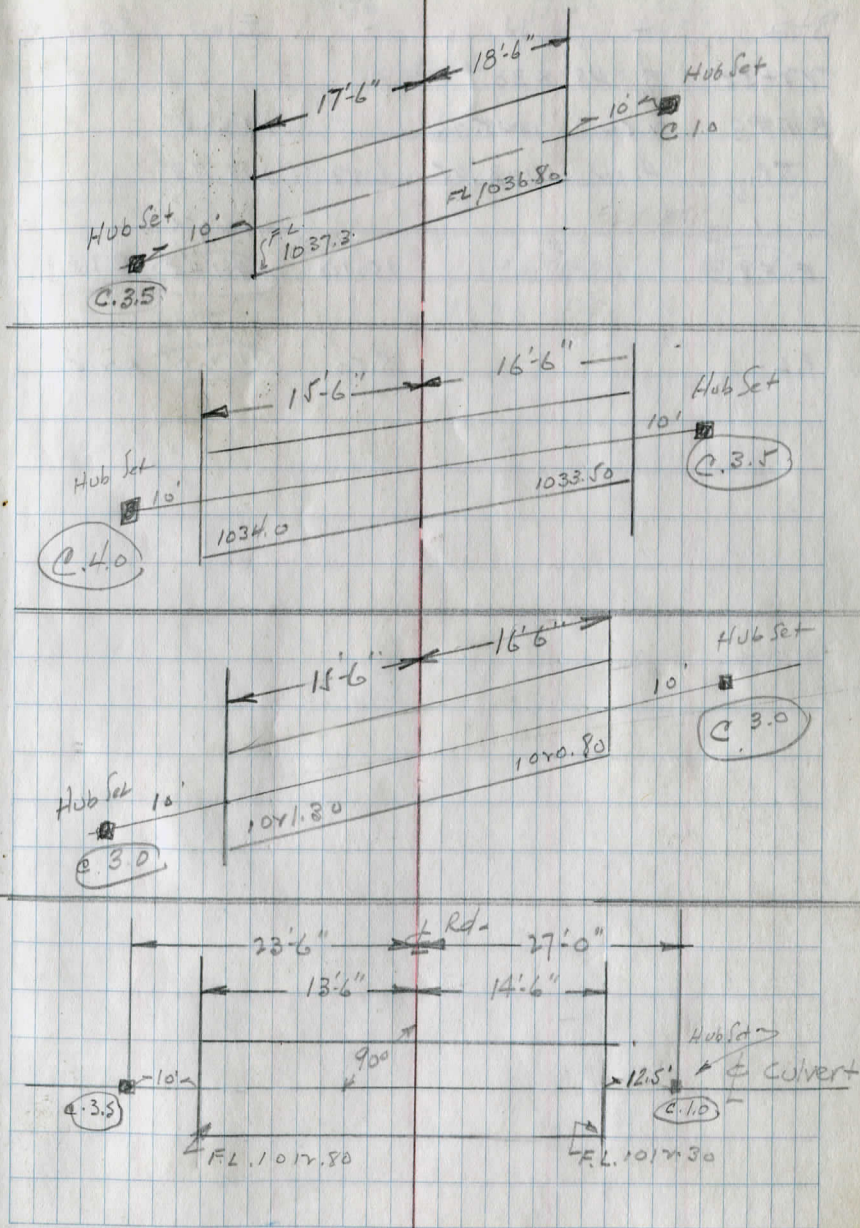
Sta	+	H.I.	-	Elev.	Rem's
81+71		28' x 22" R.C.P.			
B.M. #9	1.20	1021.28	1020.08		
E Hub			8.16	1014.12	C.1.0
				1013.12	
W Hub			4.80	1014.92	C.3.5
				1016.48	

W

E Rd-

E

(35)



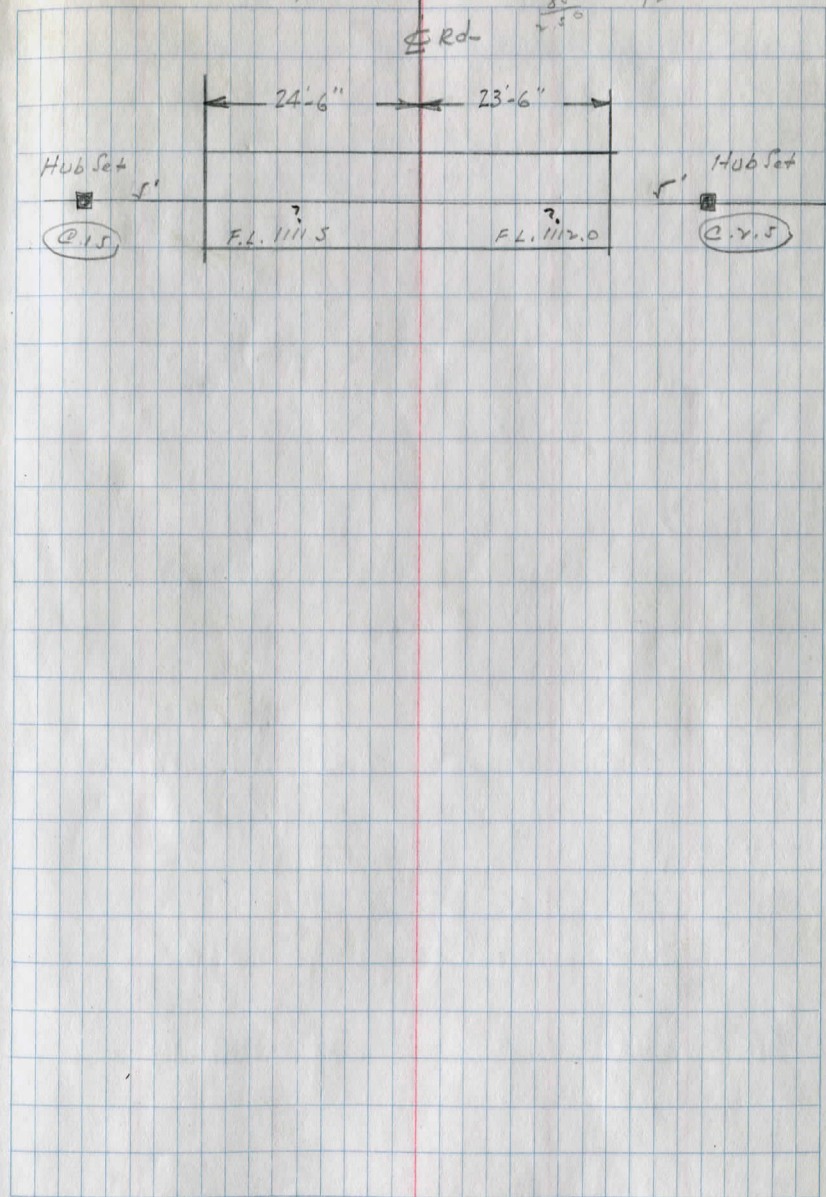
Sta	+ H.I.	-	Elev.	Remarks
22455	48' x 30" R.C.P.			
B.M.#3	2.52	1125.76	1123.24	
T.P.	4.12	1123.05	6.83	1118.93
			1112.95	
E.F.L.		10.10	1111.45	C.I.S
			1114.55	
W.F.L.		8.50	1114.05	C.I.S

23.05
11.45
11.60

23.05
12.05
11.08
8.50
2.50

23.05
10.50
12.55

(36)



Sept. 29, 1936 Garrison Cor N. Rd.

Sta	+	H. I	-	Elev.	Rem
B.M.#2	7.11	1155.45		1148.34	
T.P.	7.62	1162.96	0.11	1155.34	
5+0					
6+0					
7+0					
B.M.#2	2.97	1151.31		1148.34	
8+0					
9+0					
T.P.	1.46	1140.74	12.03	1139.28	
10+0					
11+0					
T.P.	13.07	1151.25	2.56	1138.18	
12+0					
T.P.	11.08	1161.84	0.49	1150.76	
13+0					
T.P.	5.33	1164.58	2.59	1159.25	
13+50					
T.P.	7.41	1168.60	3.39	1161.19	
14+0					
T.P.	5.87	1165.62	8.85	1159.75	

S. Gould Jr.
Geo. Dietz

38

West	Elev.	East
C. 3.0 <u>23'-9"</u>	1159.15	C. 1.0 <u>21'-0"</u>
C. 3.0 <u>23'-6"</u>	1156.95	C. 1.0 <u>21'-0"</u>
C. 9.0 <u>32'-0"</u>	1152.30	C. 3.0 <u>23'-0"</u>
C. 10.0 <u>29'-0"</u>	1147.30	Gr. <u>19'-6"</u>
C. 7.0 <u>28'-6"</u>	1142.78	F. 3.5 <u>22'-9"</u>
F. 10.0 <u>32'-0"</u>	1141.58	F. 7.0 <u>28'-0"</u>
F. 12.0 <u>32'-0"</u>	1144.18	F. 6.0 <u>27'-0"</u>
C. 6.0 <u>29'-6"</u>	1150.10	Gr. <u>18'-0"</u>
C. 9.0 <u>30'-9"</u>	1156.50	C. 6.0 <u>26'-0"</u>
C. 5.5 <u>27'-8"</u>	1158.95	C. 1.0 <u>20'-5"</u>
C. 3.0 <u>23'-3"</u>	1159.90	Gr. <u>19'-8"</u>

Sta	+	H.I.	-	Elev.	Rem's
		1165.62			
15+0					
16+0					
16+50					
17+0					
T.P.			5.81 (side station)	1159.65	Top E.Hub Sta 17+0
18+0					
B.M.#3	5.55	1128.79		1123.24	
19+0					
T.P.	7.68	1125.12	11.35	1117.44	
20+0					
T.P.	12.30 ³¹	1137.01	0.41	1124.71	
21+0					
T.P.	13.00	1149.53	0.48	1136.53	
22+0					
T.P.	12.61	1161.66	0.48	1149.05	
23+0					
T.P.	9.44	1138.03	0.20	1128.59	
24+0					

39

West	± Elev.	East
C.2.0 22'-3"	1160.30	F.1.0 16'-9"
C.3.0 23'-6"	1160.21	C.0.5 20'-6"
C.4.0 26'-3"	1158.92	C.2.0 22'-0"
C.6.0 30'-0"	1156.65	C.3.0 23'-6"
C.10.5 37'-0"	1149.63	C.5.5 28'-0"
C.9.0 32'-0"	1142.11	C.6.0 28'-6"
F.0.5 18'-9"	1134.59	F.0.5 20'-0"
F.5.5 27'-0"	1127.08	F.4.0 24'-3"
F.5.0 25'-0"	1121.92	F.4.5' 23'-6"
	1121.06	
C.5.0 26'-9"	1121.45	F.4.0 22'-6"
C.11.0 31'-9"	1125.70	C.3.0 22'-6"

Sta	+	H.I.	-	Elev.	Rems
		1138.03			
25+0					
T.P.	5.81	1142.55	1.29	1136.74	
26+0					
26+50					
27+0					
T.P.	0.70	1131.64	11.61	1130.94	
T.P.	0.85	1121.86	10.63	1121.01	
B.M. #4			6.47	1115.42 rec. 1114.39	

West	± Elev	East
0.5.5 22'-6"	1132.30	0.2.0 22'-0"
0.5.0 21'-3"	1136.74	Gr. 20'-0"
0.5.0 20'-9"	1137.34	0.1.0 20'-8"
0.4.5 20'-3"	1136.86	Gr. 20'-6"

Thompson Rd (E. of 528)

Patterson
Franks & Carfield N

June 30 56

8+40
 7+40 Ditch 15' CEI No# 18' off E
 6+00 18" Wild Cherry 30' off 40" Maple 30' off
 5+80 24" Conc Culvert 33' long 15' off CEI No# 20' off E
 Geod - Clear
 5+00 20" Maple Ditch 16.5 19'
 18" Maple 16.5
 16" Maple 16.5
 20" Maple Ditch 16.5 19'
 CEI Pole No # 21' off E
 3+90 20" Maple Ditch 16.5 19' Clear

S
Twin Maple 27'
18" Maple 29'

40" Maple 20'

Ditch 15' CEI No# 18' off E

40" Maple 30' off

CEI No# 20' off E
Ditch

20" Maple Ditch 16.5 19'

18" Maple 16.5

16" Maple 16.5

20" Maple Ditch 16.5 19'

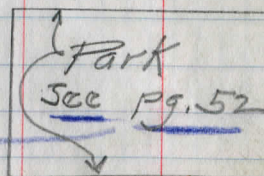
Red go maple 29'
20" Maple 29'

CEI Pole No # 21' off E

20" Maple Ditch 16.5 19'

Clear

E 528 (North) 0+00



Sta 14400 E No Ditch
 11+00
 13+70 8" x 16" Conc IP With Conc Hdws 15'
 CEI No# 18'
 13+00 18" Maple 30'
 18" Maple 28'
 18" Maple 29'
 Ditch 15'
 12+15 Twin maple 29'
 11+70 18" Maple 28' CEI No# 15'
 11+0
 10+36 Drive Culvert 8" x 21" Conc Pipe with Hdws 15' Ditch 15'
 Ditch 14' CEI # 89130 20'
 ? 8" Drain Tile 1/3 Full
 9+34
 9+00 Ditch 15' Ditch 15' CEI No# 19'

Sta 12+70 - 14459 No Ditch

Drive Culvert 8" x 21" Conc Pipe with Hdws 15' Ditch 15'

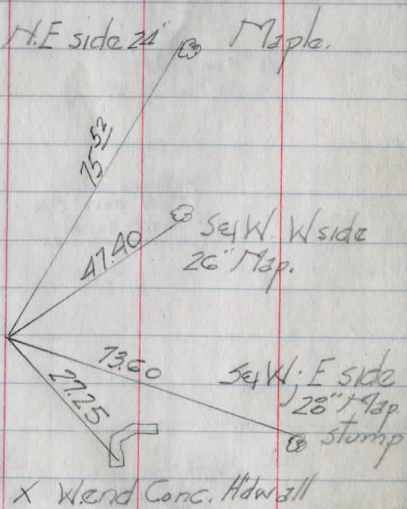
Ditch 14' CEI # 89130 20' ? 8" Drain Tile 1/3 Full

6/19/40 Pomeoy - Richards - Hosford 11 AM

7.4.49

Mosley Road Sec B

Se W. H.E side 24' @ Maple.



+22 24'x40' Enc VSP Culit.

0+00 Spk W set

6+32.5 28" x 15" x 21 Stone Culit. Nearly plugged.

- 3' - 18' - Fair cond.

4" VSP overflows
± 25'

6+50 End brush

6to

5to

4to

+27 25' @ 16" M

3to 15' Bag brush

+80 26' @ 20" W.Ch.

+48 28' @ 20" M

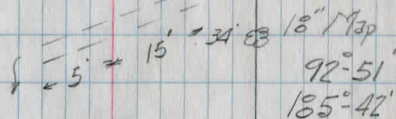
+07 27' @ 10" M

2to

+65 30' @ 16" M

1to 35' @ 24" M

+69 24'x20" Wood box culit



Middlefield

15' - 25.5'

Madison Road

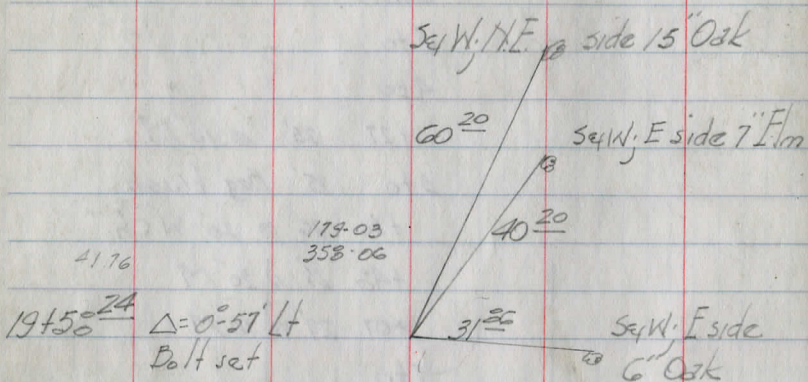
20' Bit. pavit

9.97

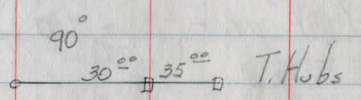
100
498.5

S.R. 528

T Hubbfd
at P.I. of culit.



10+30⁴⁴ P.O.T.
Bolt set



26+0	*	
+40	rock	bot croops
25+0	*	
+40		side ditch
+35	9'	ditch centers from S
+10	19'	10" Oak
24+0		
+95	26'	15" Oak
23+0		
+25	26'	10" Oak
22+0	+50	18' 20" Oak
21+0	*	
20+0		
16.5'	x	dead pipe
19+0		
18+0		
17+0		
16+0		
15+0		
14+0		
13+0		
12+0		
+50	16	Brush
11+0		
10+0		
9+0		
8+0		
+80	25'	Big brush

Approx lat
Line P.L.

rough stone
drive Culvert
No Good

+85

+73 < 15' >

+06

10.5' □

x < 26' > 32 + 0 < 15' >

+85

+67

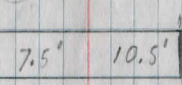
< 25.5' > 31 + 0 < 13' >

+74

RISE 15" Walnut

Rock pile 10' + 25'

+05 4'x4' Conc. Box
Very poor cond.



24' 30 + 0 17'

+87 17' 6" Ash

+64 26' □ 15" Ash

+40

+20 17' 6" 15" Maple

12" Maple

+5

< 23' > 29 + 0 < 14' >

+89

12" Maple

27 29

28 + 0

27 + 0 16'

Very bad ditches
Both sides of bridge

Sta.	+	H.I.	-	E
BM #4			3.61	1047.07 (1047.01)
T.P.	3.53	1050.68	12.95	1047.15
T.P.	0.91	1060.10	12.93	1059.17
+87.17				1067.42
37+0				1065.42
36+0				1067.82
+74.5				1065.12
T.P.	6.31	1072.12	12.02	1065.81
35+0				1066.43
34+0				1073.43
T.P.	1.30	1077.83	11.69	1076.53
33+0				1077.82
32+0				1083.21
BM #3	0.37	1088.22	6.36	1087.85

1094.21

Spk. H.E. Root 4" Ash + 600' H of intersection
W side of Garrison & H. Road.

			9.3		4.7		1.9	
			100		E		100	
7.6	5.9	7.4		6.7	6.8	7.5	6.7	2.7
30	12	10		E	6	7	10	17
						8		20
								30
10.6	7.9	8.3	7.6	7.3	7.6	7.9	7.5	6.7
30	12	10	8	E	8	10	11	20
			9					30
14.0	12.4	9.1	10.8	7.0	10.0	8.6		
100	50	Top	FL	E	FL.	Top		
		op						
13.5	11.9	12.2	11.6	11.4	11.4	11.9	12.0	10.5
30	15	14	11	E	4	6	9	30
		13						
3.5	3.0	5.0	4.5		4.4	4.5	5.1	5.0
30	19	14	11		E	5	6	8
		13						17
								30
8.7	8.7	10.8	11.1	11.6	10.4	10.5	10.4	10.7
30	22	15	13	12	10	E	7	9
				11				15
								30
5.5	5.1	6.0	6.2	5.3	5.1	4.5	5.4	3.1
30	18	16	13	9	E	8	10	14
							11	20
								30

Spk. H.E. Root 15" Walnut Sta 30+74 Rt 22'

MOSELEY ROAD

Culvert stakes

B.M. 4.52 1044.75 1040.23
 1040.00 ± Gr.

S stk
 7.50 1037.25 FL.
 2.50 1042.25
 C 5.00

N stk
 8.00 1036.75 FL.
 6.00 1138.75
 C 2.00

B.M. 5.22 1045.45 1040.23

S stk
 5.75 1143.20 ± G
 3.25 39.70 FL.
 C 2.50

N stk
 6.25
 4.50
 C 1.75

B.M.#3 4.06 1091.91 1087.05

S stk
 9.91 FL 1087.00 ± Gr.
 3.41
 C 6.50

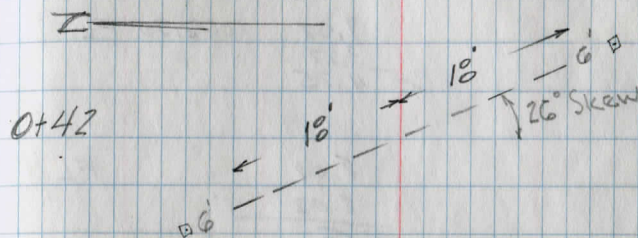
N (bolt in rock)
 11.28 FL.
 10.41 FL.
 F 0.89

10/16/40

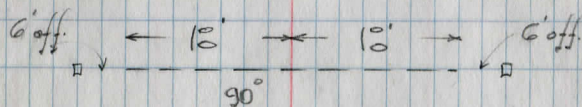
Pomerooy
 Richards
 Patrik
 Vaccarillo

50

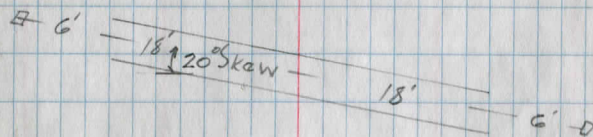
Adviall 0-29 Pt.



0+32.5 18' x 36' Corr. I.P.



N.E. root 15" Wal. 22' Rft of 30+74
 30+03 5' x 4' x 36' Conc. Box



1091.91

T.P. 0.26 1079.78 12.39 1079.52
 1066.00 \neq Gr.

T.P. 3.37 1070.02 13.13 1066.65

S stk 7.52 1062.50 FL.

$\frac{3.27}{4.25}$

Nstk 8.02 FL.

$\frac{8.02}{9}$

35+74⁵ 18x36 Corr. I.P.

6 — 18' — 18' — 6-0 12° Skew

Sta 20 sat. 11' S of E
 Sta 19 sat 12' S of E

376.0

Sta 18+0 sat on C.

Top end guard post
 Nail N. side 3" dn Fd 6/58

Sta 17+88.39 P.I. $\Delta = 16^\circ 28' 00''$

S&W. W. side
 C.E.I. Pole # 55272

Boat Spk. Sat
 Fd. 8-54
 Spike W side
 Walnut 4 up
 Fd 7/66
 ravel 79' 3"

Sta 17+0

328.5

Sta 16+0

S&W. N.E. side C.E.I.
 Pole

re-ref. Fd 6/58
 " 4/66

Sta. 14+59.90 P.I. $\Delta = 28^\circ 00' 00''$

S&W. W. side 24" Zap. 35 48

Bolt. Sat.

S&W. Fd 5' 6" 8-54

Sta. 13+75 Rock Bag.

S&W. N.W. side 10" Zap.

20+70 End Bathing Pits

12' x 2' GUARD
 12' x 2' GUARD

18+80 G.R. Bag.

197' < 8' >
 18' of trail Rd.
 18' Ext ±
 133° 32'

15+30 < 30' > End Rock axis

End rock on N. 15' x 25'
 14' 14.5' on Rock

16+0 Cross on Rock 14.5' 12.5' Cross on Rock

15+25 Summit
 8" Core I.P. Conc. Hd/s
 18' 2 1/8" 11+0
 8" Core I.P. Conc. Hd/s
 13+75
 10+45
 11+5
 9+43
 6" V.S.P.
 conc. ditch curb

Ed. 4/66
re-ref

SPL N.W. Side
828785

PROBABLE CULV. STATION, P.I. = 21+74.20

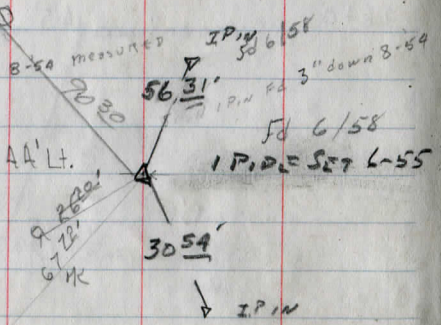
Sta. 21+64.11

$\Delta = 21^\circ 44' \text{ Lt.}$

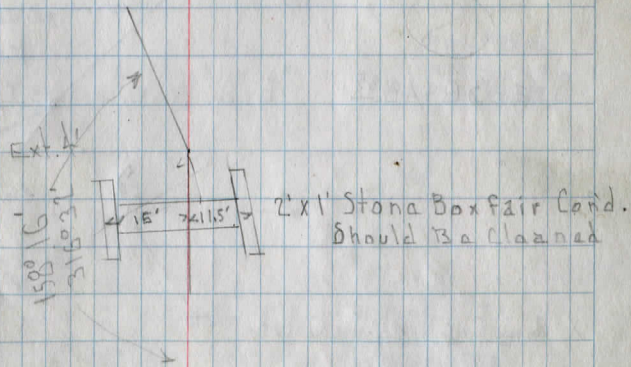
S&W. W. Side of Pole
G.M.C.

376.0

S&W. W. Side
C.E.I. Pole # 565224

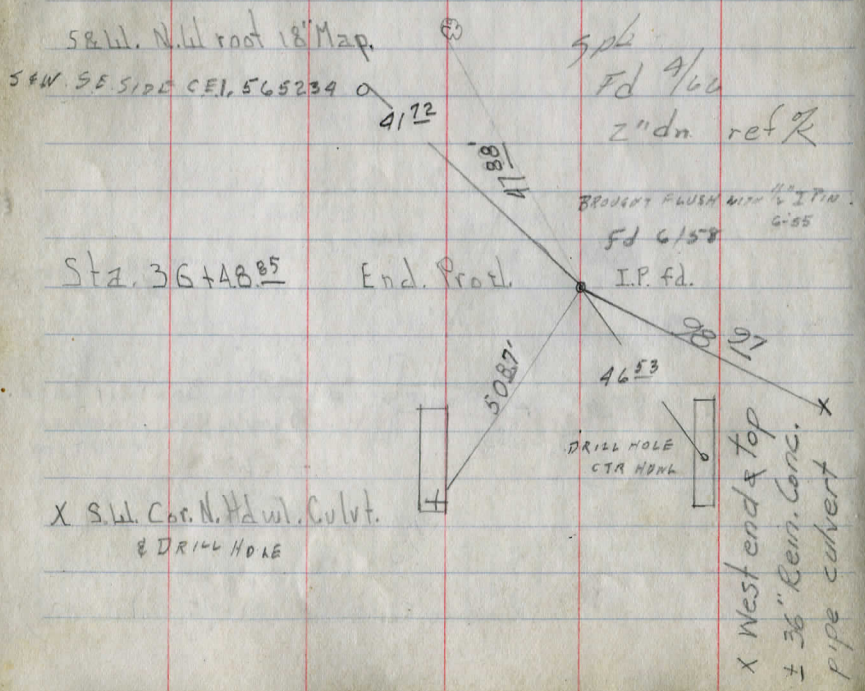


Stk. Sta. 21+0 set 30'S off All Sta. E of 21 set 30'S



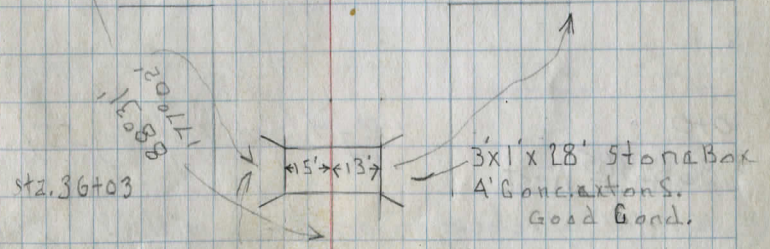
Stone in Rd. Ends 21+0=

See BK 14 pg 4.
Topo & levels



CH. 742
Under Ledge

TM. #56
Road



CH #7

6+60

124/400 ³

4+48⁸⁵ P.O.T

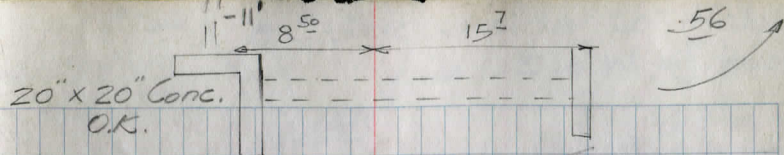
SEPT 44
Pomeroy & Co.
THOMPSON CENTER
ROAD SEC. G-H

0+0

= 36+48⁸⁵ West

= 36+21.11 by relocation on ledge hill

I.P. fd (sec ref. pg 55)



CEI

565237

Spk

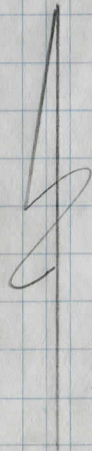
Spike H.
side 60"
Osk

install 24' pipe

Spk 5402
June, 1959

Spike set

EAST



Monument Set
July 1966

outlet ditch
needs opening

0+33

18'

12" Conc.

UNDER 179-50

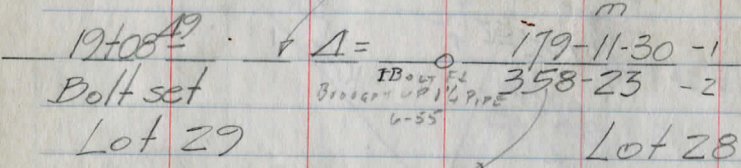
LEDGE
ROAD

12' gravel
32' ditches

14' gravel
32' ditches

0 21+64⁴¹

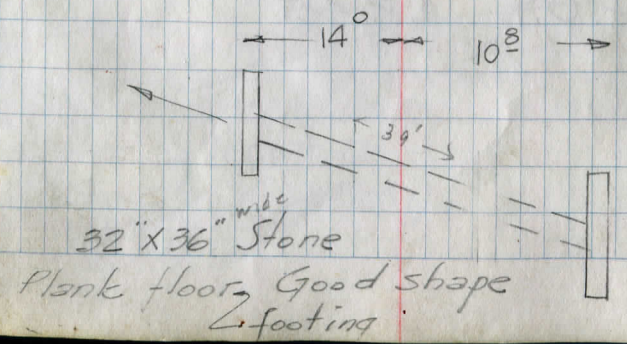
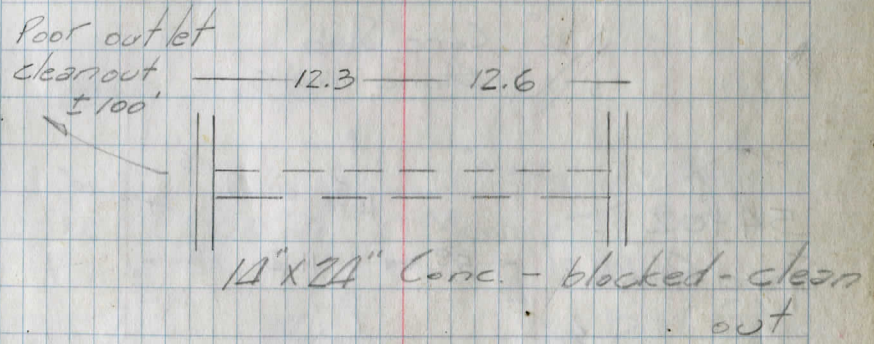
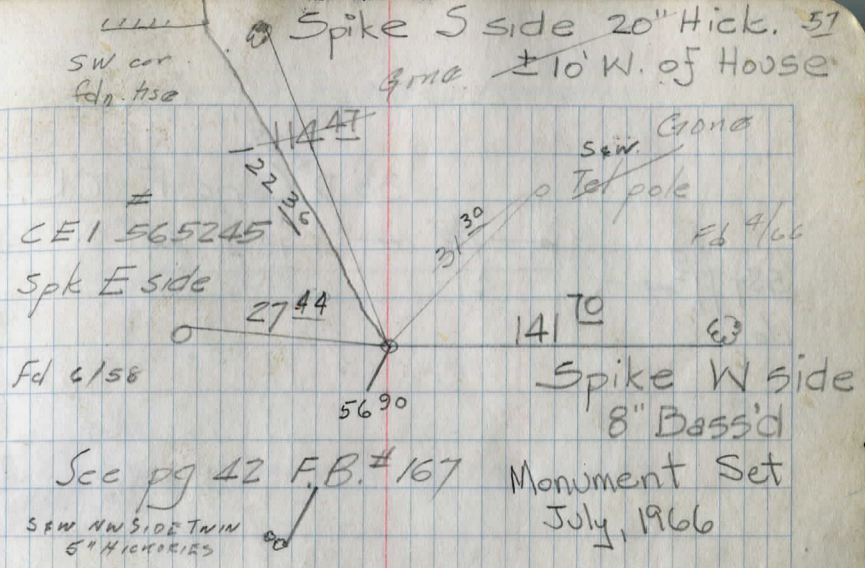
Lot 32 ± Lot line ← Lot 33



55+29.6

17+70

16+55.5



58+90 23'RT (NW Cor Headwall)

58+00 18'
57+00 18'
56+00 20'RT

44+00 to 55+00 stks 18'RT

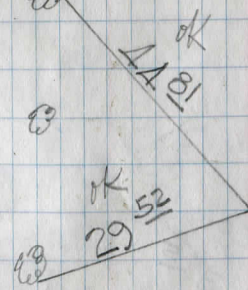
44+00 13'RT

FD 8" dn. 9/66

Spike SE side 24" Maple

Monument Set July 13, 1966

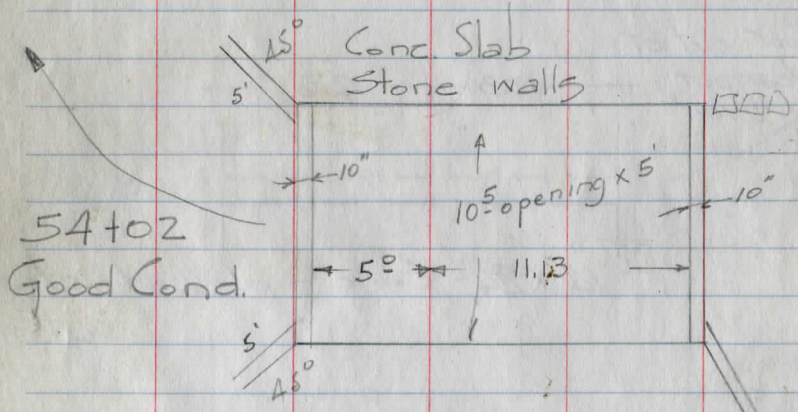
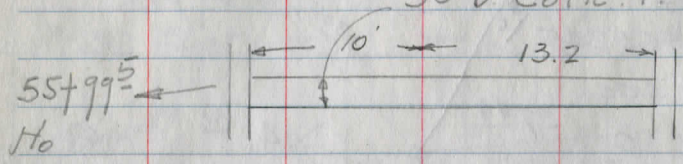
B.M. Spike N.W. root



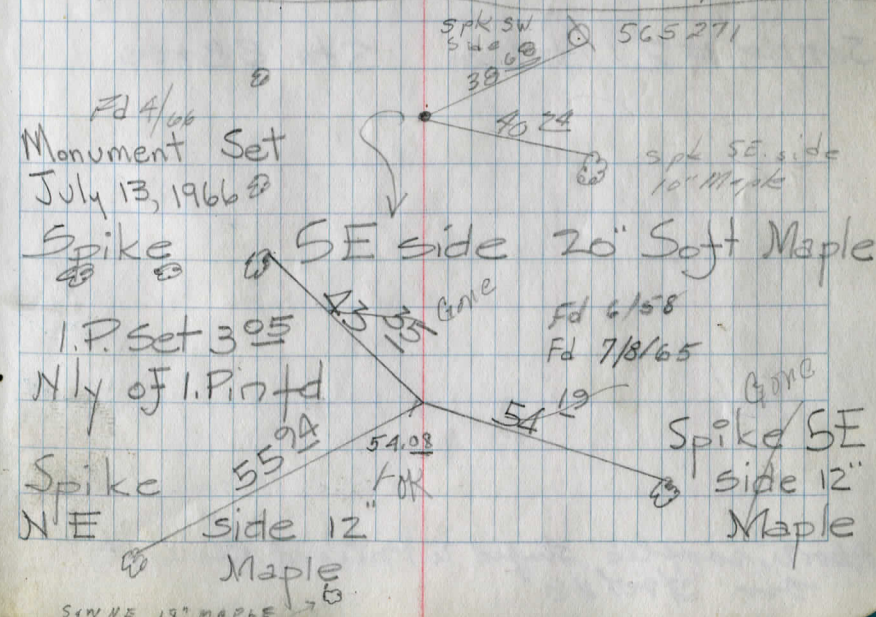
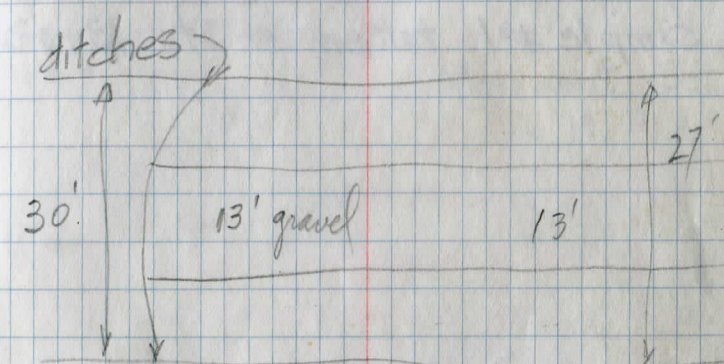
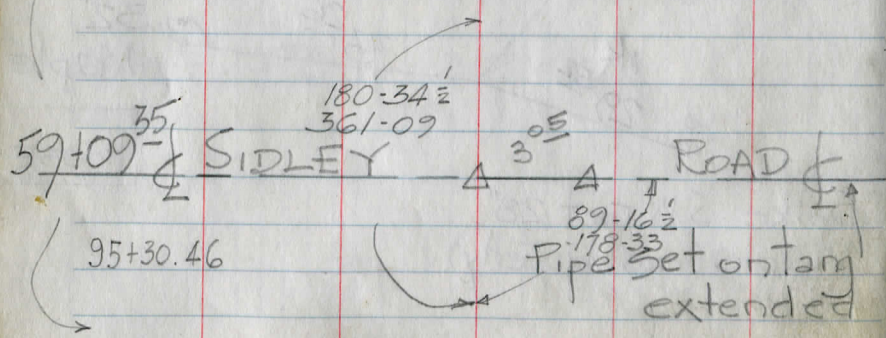
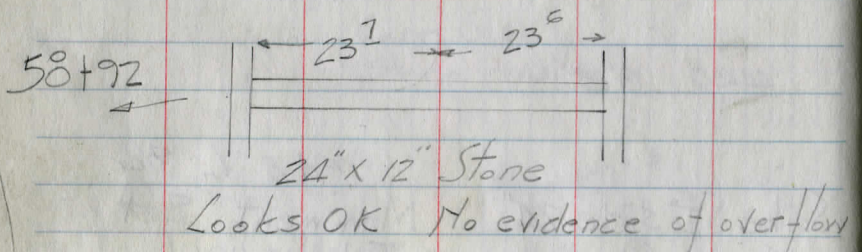
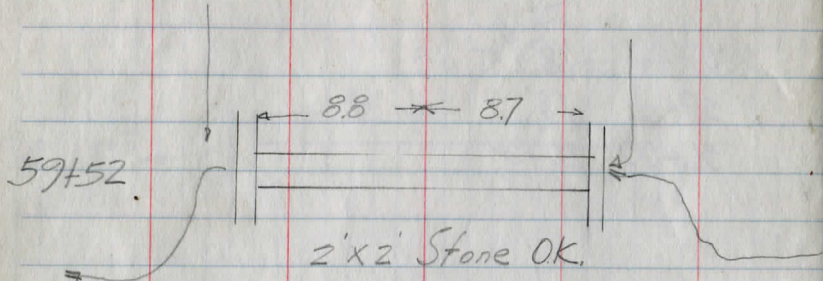
HOUSE

Spike SW root 28" Maple (most westerly)

30" D x 28' Conc. P. OK.



33+00.00 P.O.T. I.P. set
69+21.11



69+65⁰⁰

105+86.11

179-45¹/₂
Δ 359-31

⊙

⊙

3/14/46

Soil sample #1 taken at Sta 13+00

Sample #2 taken Sta 88+00

Above 2 samples shipped to Portland Cement
Co. 3/20/46

Spike N.W. Side 20" Soft
Maple 60

55⁴⁸/₁₁

Spike E side

18" Soft 45⁹²/₂

⊙ Map. 46⁰⁹/₆

42¹⁷/₁₁

^{gone}
B.M. Spike 42³³/₁₁

S.W. root 18" Hemlock

vert. spk

18" Hemlock

I.P. Set

fd 6-58

spk fd 4/66 4" dn

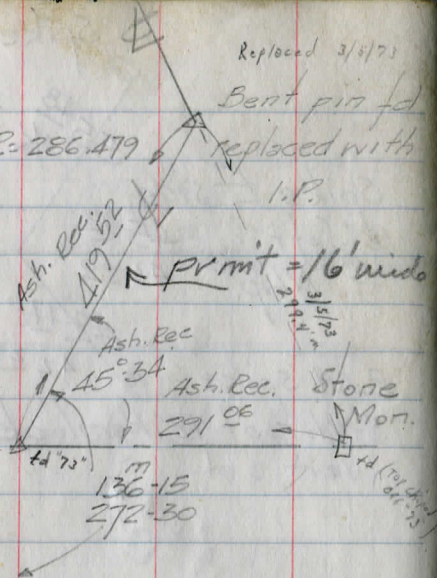
re-ref.

Monument Set
July 13, 1966

NO MON FD. 8-21-84

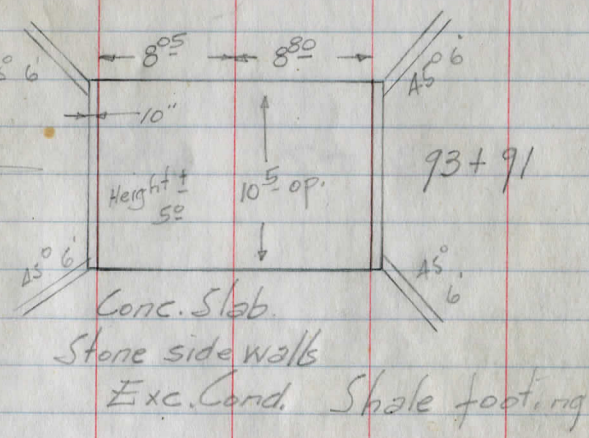
Ash. Rec. Our.
 $\Delta = 43^\circ 44'$ $\Delta = 43-45$ R. 286.479
 $D = 20^\circ$ $D = 20^\circ$
 $E = 22.21$ $E =$
 $T = 114.98$ $T = 115.02$
 $L = 218.67$

Replaced 3/4/71
 Bent pin fd
 replaced with
 I.P.



ASHT. Co.
 GEA. Co.

- 96+48¹⁵
- 132+69.26
- 01-41 1087
- 04-11 2517
- 06-41 2517
- 09-11 2517
- 11-41 2517

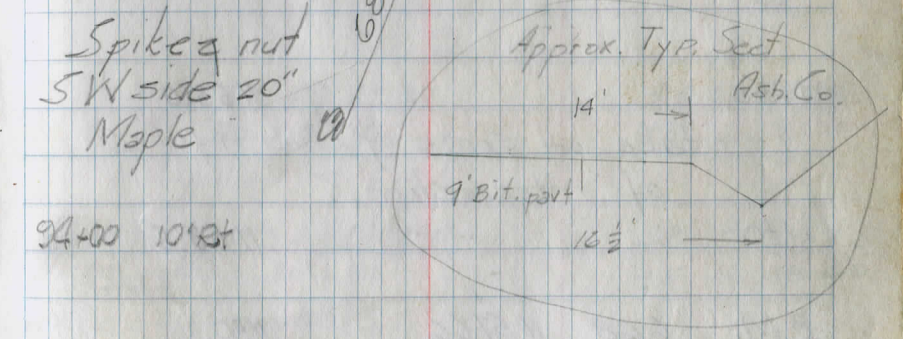


80+27²³

Spike
 H 85° W

Spike & nut N side 22" Soft Maple
 ← Barrett Ed #70
 (in Ashtabula)

Spike & Washer
 SE side 18" Maple
 96+45 Beg. Bit.
 Mac. east
 Feb 6/58 Feb 4/66 16" dn
 I. Pin fd 1' below
 Surface
 Fd 6-55
 DRAWS RED NEEDLE
 Ed. 5-73



B.M. Spike SE root 15" Maple

Spike SW side
 13" Maple @ 26⁴⁸

Spike SW
 side 15" Maple @ 34¹⁶

Spike set P.O.T.
 + 150 East of
 house

9-30-44
 Hall - Wilson
 Pom - 3:00 P.M.

SECTIONS H=7

	+	H1	-	E
4+0				1145.7
T.P.	0.98	1149.18	9.46	1148.20
3+0				1149.1
2+0				1151.7
1+50				1153.0
take off some of knob & fill S of intersection?				
1+0				1153.5
B.M.	6.68	1157.66		1150.98
0+30	Culvert			
0-250				1156.2
0-200				1053.9
0-100				1051.3
0+0				1051.0
B.M.	5.43	1156.41		1150.98

NORTH SOUTH

1.9	1.5	4.5	5.1	3.5	4.4	2.0	1.7	2.3	
30	23	17	15		13	19	23	30	
					15				
		7.0	10.0	8.6			9.7	6.7	
		22	15				14	21	
		30						30	
		5.7	5.6	7.5	6.0		6.9	5.0	
		30	19	14			17	21	
								30	
		5.0	4.8	6.2	4.7		5.6	6.2	
		30	19	13			13	16	
							18	30	
taken in drive									
		3.4	4.1	4.15			4.8	5.1	
ditch both sides							11.5	16	
		30	11				18	30	
bank ± 3.4 drive west									
		7.54					± 7.5	outlet plugged	
		FL					FL		
					0.2				
					2.5				
					5.1				
		1.2	2.6	5.4	5.9	10.2	10.3	6.3	
		150	100	15	100	110	200	250	
x SW. & N. hdwl west of intersection with Under Ledger Rd									

	+	H.I.	-	E
T.P.	5.83	1108.71	7.55	1102.88 ✓
16				1106.1
T.P.	1.30	1110.43		1109.13
15				1107.5
T.P.	2.50	1111.63	8.18	1109.13 ✓
14				1109.5
13				1112.1
B.M.			4.31	1113.00 ✓
1240				1115.2
T.P.	0.41	1117.31	10.58	1116.90 ✓
1140				1118.5
1040				1123.13
T.P.	0.12	1127.48	11.43	1127.36 ✓
940				1128.8
		1138.79		

HOETH SOUTH

H.W & H. Hdwl culvt 17±70

3.0 3.9 5.6 5.0 4.3 5.3 6.8 6.6 5.5 5.1 5.2
60 50 46 42 30 20 18.5 15 13 8 0

4.4 4.1 5.3 5.9 5.1 4.6 4.5
44.5 30 17.5 14 13 7 0
60 16

6.0 6.1 8.3 8.5 8.9 7.8 9.1 9.6 8.8 7.5
60 55 50 47 46 30 17 13.5 12 0

+1.0 4.6 6.5 6.1 5.2 6.3 7.0 7.2 6.3 7.4
55 50 43 42 30 18 16 13.5 11 0
60 45

Spike N.E. root 20" Map. Sta. 12+33 Rt+26'

+5.0 3.1 3.3 2.9 2.1 3.5 4.4 3.9 4.9
55 45.5 43.5 42.5 30 17.5 13.5 12 0
60 15

3.6 3.4 7.4 10.2 9.7 9.0 10.1 10.7 9.1 10.1
60 54 50 44 41.5 30 17.5 14 10.5 0

+0.9 +0.7 4.8 5.3 4.9 4.35 5.3 5.5 3.7 2.9 3.0
60 50 45 42 40 30 18 15.5 12 7.5 0
43.5

7.0 7.8 10.4 10.1 10.0 10.7 10.6 9.5 10.1
60 48 43 39.5 30 16 14 11 30

£

T.P. 0.68 1198.41 7.81 1097.73

20 1098.2

19 1100.7

T.P. 2.66 1105.54 1102.88

18 1101.9

17770 Cult. 1102.4

T.P. 4.50 1107.38 1102.88

17 1103.8

16+55⁵ Cult 1105.4

1108.71

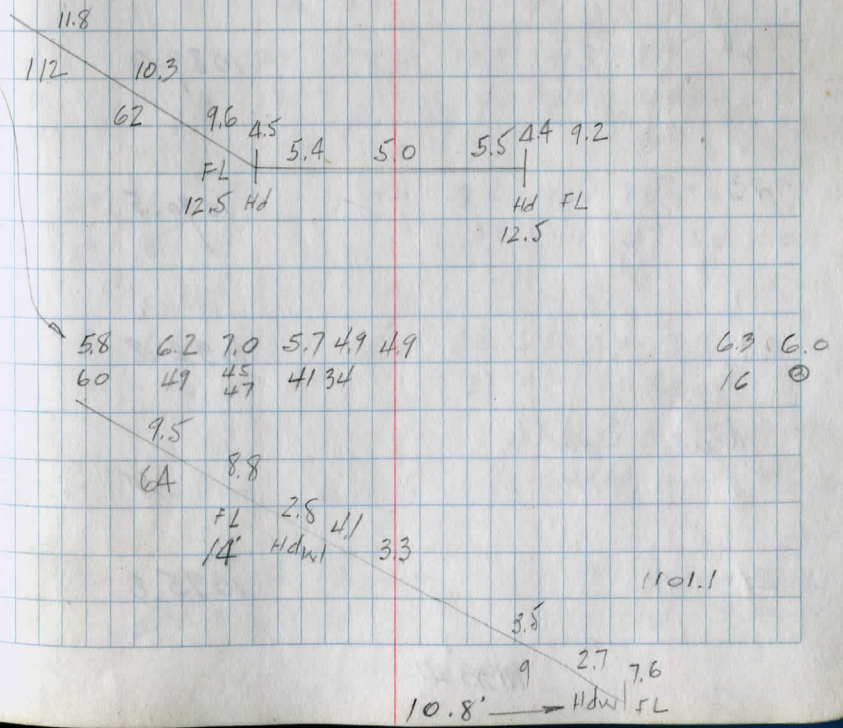
6.3 7.3 8.2 7.7 7.3 8.0 8.4 6.0 6.3
60 50 44 39 20 16 10 0
18

4.0 3.7 6.9 5.4 4.8 5.4 5.7 3.8 3.0
60 54 42 38 19 16 11 30
44

9.9 8.7 6.2 5.5 6.1 7.9 7.5 4.5
60 46 39 20 17 11 0

11.3 H. 1.0738
114

See F.B. 167 pg 42



1101.1

28

1085.5

27

1086.2

D.M

4.46

1087.09

26

1087.0

25

1087.85

T.P.

2.49

1091.55

9.35

1089.06

24

1089.0

23

1090.5

22

1092.8

drive South

21

1095.8

1093.41

7.0 7.0 7.7 6.8

0 11 13 16

6.1 6.9 8.4 7.5

39 43 50

60

6.4 6.1 7.1 6.1

0 11 12 16

5.4 6.3 7.0 6.7 6.3

40 44 47 60

Spike SE foot 26" Soft Map. 26+88 So. + 32'

5.3 5.0 6.0 5.4

0 11 13 17

4.6 5.5 5.9 5.5 5.3

39 42 46 60

4.2 4.3 5.1 4.5

0 13 14 17

3.7 4.7 5.4 4.6 4.3

40 42 47 50

60

10.1 9.8 10.7 10.2

0 11 14 17

9.4 10.4 11.3 9.9

40 44 49

60

8.0 7.9 9.3 8.5

0 13 15 18

7.9 8.6 9.4 7.5 7.4 7.7

39 44 47 50 60

4.1 4.1 6.6 6.1

0 13 16 19

5.6 5.8 6.6 4.0 3.9

37 43 50 60

6.3 5.5

outlet inlet

2.1 2.0 3.7 3.3 2.6

60 47 42 40

3.4 4.0 1.7 1.1

21 18 10 0

37

1067.0

T.P.

0.92

1074.13

8.80

1073.21

36

1069.5

35+5

✓

1073.1

34

1077.5

B.M.

1.58

1082.01

8.08

1080.43

33

1080.7

32

1082.4

31

1083.6

30+0

T.P.

2.17

1088.51

5.21

1086.34

stk 29

29+0

1084.8

1091.55

4.1

4.2

8.4

8.0

7.1

8.3

9.3

7.8

7.2

7.0

0

5

13

16

39.5

41.5

44

47

60

9.1

9.9

13.8

13.0

12.5

13.5

13.7

15.0

13.8

12.7

12.9

0

5.5

11

17

38

40.5

41.5

43

47

60

4.6

4.7

10.5

9.0

8.8

8.9

9.8

11.3

9.5

7.7

8.7

0

5

11

16

27

30

38

41

45

50

60

1.6

2.1

6.2

4.8

4.3

4.5

5.4

5.9

3.5

4.0

0

6

10.5

15

26

37

40

41

46

52

60

Spk N. W root 36" Map. ± 75' South Sta. 33+10

5.5

5.6

10.2

8.2

7.6

7.8

8.6

9.7

8.9

7.9

7.5

0

6

11

16

20

37

40

44

46

60

4.7

4.8

8.3

6.6

6.0

6.1

6.9

8.7

7.8

6.1

6.5

0

6

11.5

15

27

30

37

41

44

47

60

4.4

4.3

7.0

5.9

4.9

5.9

7.6

5.4

5.9

0

7

11

14

39

41

47

60

3.6

3.8

5.9

5.0

4.4

5.2

6.6

4.6

5.1

0

8

12

16

39

42

49

60

6.6

7.2

8.4

7.4

6.8

7.7

9.1

7.5

7.9

0

11

13

16

40

43

46

60

45 1057.1

T.P. 0.94 1058.87 743 1057.93
44 1058.6

43 1059.4

42 1060.4

41 1061.3

40 1062.1

T.P. 1.37 1065.36 10.14 1063.99

39 1063.4

38 1065.1

1074.13

1.6 0.8 0.9 3.9 2.9 1.8 2.8 4.6 3.0 0.4
0 8 12 15 18 41 43 46 51 60

7.5 6.8 7.3 8.9 7.9 6.8 7.9 9.1 7.7 6.1 5.4
0 8 12 14 17 30 41 44 46 50 60

7.2 6.3 6.6 7.2 6.8 6.0 7.2 8.2 6.6 5.3 5.2
0 9 13 16 18 40 43 45 49 60

6.6 5.5 5.6 6.2 5.8 5.0 6.0 6.9 5.5 4.9 4.6
0 9 14 15 18 39 43 45 48 60

5.2 4.6 5.4 5.0 4.1 4.9 5.9 3.8 4.0
0 13 15 18 39 43 49 60

3.9 3.4 4.4 4.1 3.3 4.1 4.6 3.4 3.2
0 11 14 17 39 41 46 60

Stk 39 ± 57 North
drive pipe

12.0 11.3
out in

11.0 10.3 12.6 11.4 10.7 11.0 12.6 10.6 10.3
0 9 13 16 36.5 40 44 46

9.3 8.9 10.5 9.9 9.0 9.1 10.3 9.6 8.9 8.7
0 9 13 16 38 41 44 47.5 60

52

1044.8

51

1046.6

PM

0.83

1049.99

50

1049.1

T.P.

1.33

1050.82

9.38

1049.49

49

1050.8

48

1052.2

47±45

R+

drive culot

47±12

L+

drive culot

47

1054.0

46±46

46

1055.4

1058.87

5.6	6.2	7.6	6.5	6.0	7.3	7.9	6.4	6.5
0	12	16	22		43	45.5	50	60
		17				47		

2.8	2.9	3.6	5.9	4.9	4.2	5.3	5.6	3.5
0	9	12	16	21		43	45	49
			17					60

Spike S.W. foot 20" Maple 50±36 North 22'

1.3	1.2	3.8	2.6	1.7	2.9	3.3	2.0	0.9
0	12	15.5	20		43	45	46	49
		16.5						60

8.5	7.8	7.9	10.4	8.8	8.1	9.2	9.6	7.7	7.6	6.9
0	6	13	16	20		42	44	46.5	48	60
			17							

6.9	6.2	6.1	8.4	7.5	6.7	7.7	8.0	5.2	5.7
0	4	13	15.5	19		4.1	4.3	4.6	4.9
			16.5						60

6.9	7.3	6.8	7.3
in	out	in	out

4.4	5.0	6.8	5.0	4.9	5.8	6.0	5.0	3.9
0	13	17.5	19.5		41	43	45	47
		16.5						60

9.2	9.4
45	70

ditch

2.5	2.1	5.1	4.3	3.5	4.6	6.4	4.3	1.8
0	9	15	18		41	44	47	52

60

60 1043.5
 59 1043.5 - 0.66
 BM. 5.13 1043.45 (1044.11)
 T.P. 6.51 1048.58 3.52 1042.07
 58 1041.4

57 1040.5

56 1040.7

55 1041.1

54+02 Culut 1042.8 12.1

T.P. 2.36 1045.59 7.59 1043.23

53 1043.5

1050.82

59+0 ELEV = 1043.4

64 58 6.7 6.0 5.1 5.8 6.8 5.7 5.5
 60 50 46 43 23 18 17 0

Spike SE Root 15' Maple ± 45' N.W. SIDLEY RD intersection

2.5 3.2 6.0 5.1 4.2 5.4 6.0 4.5 4.1
 60 50 45 41 19 14 11 0
 16

6.5 5.9 6.6 6.0 5.1 6.1 7.3 5.5 5.3
 60 50 43 40 18 13 10 0
 15

ditch running N at 55+0 W ←

8.1 8.3 Fault
 ±100 ±30

Note: No channel north.

6.4 5.1 9.0 5.3 4.9 5.3 8.5 8.3 5.1 5.9
 60 49 44 40 19 FL 12 9.5 0
 FL 40 17

6.4 6.7 8.0 5.6 4.5 5.5 7.4 5.5 5.1
 60 50 46 40 18 11 8 0
 47 13

36.5
 11.2 10.5 9.1 3.75 9.1 1.3 2.6 2.8 2.7 1.3 9.0
 180 130 80 top FL Hd Hd F.L.
 op. 5 11

7.8 8.4 9.7 8.0 7.3 8.6 9.4 8.1 9.1
 0 12 16 22 44 47 50 60
 17

69

1050.7

68

1051.2

67

1050.5

T.P.

6.04

1055.58

3.28

1049.54

66

1049.4

65

1048.8

64

1048.3

63

1047.4

62

1045.2

T.P.

804

1052.82

3.80

1044.78

61

1044.0

1048.58

5.2 4.6 6.3 5.8 4.9

60 50 45 42

5.9 6.3 5.4 5.2

20 18 15.5 0

4.6 4.8 5.5 5.0 4.4

60 48 46 42

5.4 5.8 4.9 4.5

20 18 15.5 0

4.9 5.0 6.7 6.3 5.1

60 48 45 43

6.0 6.3 5.2 5.0

20 18 15 0

3.1 4.9 4.3 3.4

50 44 42

60

4.2 4.5 3.2 2.4

21 18 15 0

4.2 3.8 5.6 4.7 4.0

60 50 45 41

4.9 5.4 4.5 4.0

21 18 16.5 0

4.8 4.4 6.0 5.3 4.5

60 50 45 43

5.4 6.1 4.6 4.6

21 18 15.5 0

6.0 5.4 6.6 5.8 5.4

60 50 45 41

6.1 6.7 5.1 5.1

23 19 15 0

6.6 5.6 8.3 7.6

60 49 42

9.0
44

8.3 8.6 5.9 5.4

22 19 15 0

6.1 5.3 6.1 5.4 4.6

60 50 46 43

5.4 5.8 4.3 4.0

22 19 15 0

17.5

77				1045.5
T.P.	1.63	1047.77	6.38	1046.14
76				1046.1
75				1046.9
74				1047.7
73				1048.2
72				1049.1
T.P.	3.12	1052.52	6.18	1049.40
71				1049.4
70				1049.9
BM		4.06	1051.52	(1051.48)
		1055.58		

0.9	2.5	3.7	3.3	2.3	3.4	3.6	2.6	2.2
60	48	45	43		21	18	16.5	0
5.8	6.6	7.8	7.0	6.4	7.2	7.6	6.7	6.3
60	47	45	43		21	19	17.5	0
5.4	6.0	7.0	6.3	5.5	5.6	6.5	7.0	6.2
60	47	45	43	34		21	19	17.5
4.5	5.1	6.3	5.9	4.8	5.9	6.2	5.4	5.3
60	47.5	45	43		21	19	17.5	
3.9	4.4	5.5	5.1	4.2	4.3	5.1	5.6	4.5
60	48	46	44	34		21	18	16.5
3.3	3.6	4.9	4.4	3.4	4.3	4.7	3.9	3.8
60	47	45	44		22	19	17	0
6.0	6.2	7.6	7.0	6.2	7.1	7.6	6.6	6.6
60	48.5	45	43		21	19	16.5	0
6.0	5.8	7.2	6.6	5.7	6.5	7.0	6.4	5.9
60	50	45	43	30	21	18	16	0
Spike S.W. root 18" Horn, 69+33								
26' Lt.								

T.P. 2.39 1035.98 ✓ 7.11 1033.59 ✓

86 1033.5

85 1034.3

84 1035.7

83 1036.7

T.P. 2.76 1040.70 ✓ 7.83 1037.94 ✓

82 1037.9

81 1039.4

B.M. 5.70 1042.07 ✓ (1042.02)

80 1041.4

79 1042.9

78 1044.7 ✓

1047.77 ✓

Spk Lt bank 86+0

7.1 7.2 8.5 8.0 7.2 8.1 8.4 8.0 7.5 7.4
5 12 16 18 38 41 43 46 60
0

6.0 6.5 7.3 7.1 6.4 7.2 7.6 7.1 6.4 6.3
0 12 16 18 38 41 42 45 60

4.0 4.7 6.3 5.9 5.0 6.0 6.4 5.9 5.0
0 11 16 18 39 41 42.5 46
Reverse 60

3.9 5.1 4.8 4.0 4.6 5.3 2.8 3.0
45 40 38 18 16 11 0
60

9.0 9.3 11.0 10.5 9.9 10.5 10.9 10.0 9.5
0 16 21 23 43 46 48 54
60

6.9 8.1 9.4 8.9 8.3 8.4 8.8 9.3 8.2 7.7
0 12 15 18 27 37 40 43 50
60

Spk SW root 16" Map H side road 150' E of Stone's house

5.4 5.8 7.7 7.0 6.4 7.1 7.6 6.1 6.2
0 11 15 17 38 40 43 60

3.8 4.6 6.4 5.4 4.8 4.9 5.5 5.9 4.5 4.4
60 48 46 42 34 22 19 16 0

2.8 3.7 4.9 4.0 3.1 3.1 4.1 4.5 4.1 3.7
54 48 45 42 35 22 19 17 0
60

94

1020.6

Bridge 93+91

1020.9 11.2
± 165

BM 3.27 1024.86 9.11

1021.59

93

1022.6

92

1026.4

T.P. 2.13 1030.70 7.41

1028.57

91

1028.4

90

1030.0

89

1030.7

88

1031.7

87

1032.7

1035.98

7.3 6.9 4.5 4.3 4.7 8.5 7.5
0 13 21 38.5 47 50
60

10.5 9.7 9.0 10.3 3.1 3.9 4.0 4.3 3.3 10.6
130 80 25 FL Hdwl Hdwl F.L.
8.05 8.8
S.W. ± S. Hdwl

7.6 10.2 10.1 8.8 8.1 8.7 10.1 10.4 10.7
0 12 15 21 38 45 51 60

2.1 2.3 5.7 5.2 4.3 5.2 5.9 4.0 4.3
0 9.5 16 19 41 46 51 60
16.5

6.9 6.8 9.3 8.2 7.6 8.6 9.0 7.1 6.9
0 10 16 19 42 45 50 60

6.3 6.5 7.9 6.9 6.0 6.5 7.1 5.9
0 11 15 18 40 43.5 46
60

5.5 5.7 6.9 6.2 5.3 6.3 6.6 5.7 5.8
0 12 15 17 41 43 45.5 60

4.5 4.8 5.7 5.2 4.3 5.2 5.7 5.2 5.0
0 13 15 18 40 42 45 60

4.2 3.9 4.6 4.3 3.3 4.2 4.7 3.8
0 14 16 18 39 42 46
60

10-21-44
 Form. Hall. Steely

Topo. Thompson Ctr. East

29' +75 *
 +41 20' ~~OK~~ 11" Map.
 +21 20' ~~OK~~ 10" Map
 3+0 21' →
 +35 20' * + ✓

29' +01
 2+0 20' → *

15" Ap \odot 22 +52
 +05 19.5 * +

No pipe reqd

up. 5' at 40' 1+0 *

12" Map \odot 24' +92
 +89 *

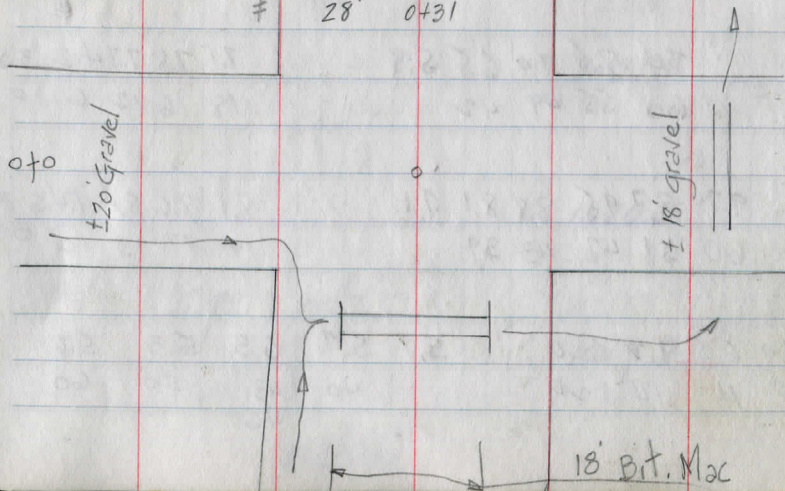
16" Map, N.G. \odot 24' +75
 ±48' +53 *

16" Map \odot 24' +42
 # 28' 0+31 *

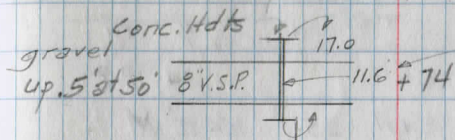
±20' Gravel

±18' gravel

18" Bit. Mac



		+43	22.5'	OK 10" M
	18" Map \odot 18.5	+40		
		+60'	+37	
	# 30'	+25		
		7+14	26'	OK 24" Oak
				6" M
		+89	22'	OK 14" M
2	17'	+80		
	gravel			
	up. 5' at 50'	8" V.S.P.	11.6'	+74
	22" M \odot 18"	+65		
		+54	19.5'	15" Ash
		6+15	17.5'	OK 12" M
		+68	17'	+ *
		+60	20.5'	OK 14" M
	# 29'	+46		
				9" M
				* 13" M
		5+08	21'	11" M
			"	9" M
			"	16" Map
		4+51	21'	* 10" M
			"	OK 13" Map
			"	OK 14" Map
		+97	21'	OK 15" Map
		+92	18'	+ ✓
		+78	21'	OK 9" Map
				*



13+22 28' ✕
 +96 29' ✕ 14" W.Ch
 +90 21.5' †

‡ 28.5' +48

12+34 25' ✕ 26" M
 +80 25.5' ✕ 26" M
 9" M
 14" M

+11 25 ✕ 12 M
 11+06 21.5' †

‡ 7" M
 13" M

‡ 29' +71

+67 24' 15" M
 + 11" M

10+09 23 ✕ 14" M
 +26 19' †

‡ † 30' +97
 9+22 22' ✕ 15" M

10" M
 † 11" M

+50 23' ✕ 15" M

8+32 ✕ 12" M

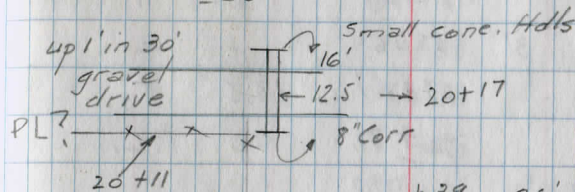
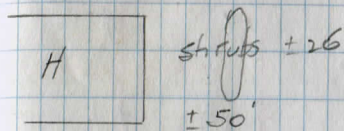
+79 22' ✕ 13" M

‡ 11" M

7+55 17.5' †

Shag Hick † 29' +73

‡ 29' +63



+39 26' ✕ west end
 +31 20' ✕ row young
 † fruit trees

← 24.5' +10

‡ 27' +10

LOT LINE

19+08.5

LOT LINE P.L.

+73 18.5' †

fence P.L. † 29' 17+60
 +75

gravel Level
 cult overflows across
 drive

+70 27.5

Heavy brush
 side 15+0
 to 20+0

‡ 25' +25 16+50 End brush South
 16+17 18.5' †

‡ 28.5 15+96

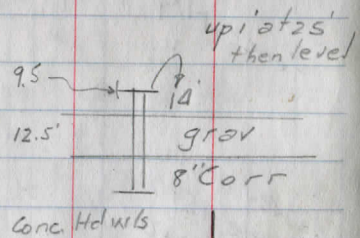
Light brush 0+0
 to 15+0
 (both sides)
 +98 28' ✕ 9" M
 † 5" M

+50 21 †

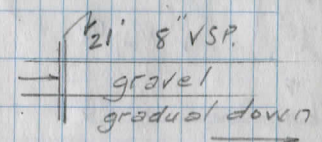
+28 27' ✕ 20" M

‡ 28.5' 14+24

±	33'	+75			
		32+20	16'	+	
±	32'	30+15			
		30+60	17'	+	
±	32'	29+39			
		29+07	18'	+	
±	31'	27+64			
		27+47	18.5'	+	
		26+75		P.L.	
±	30'	+90			
		25+61	19'	+	
±	29	+15			
		24+06	18'	+	
±	29	+62			
		+63	19.5'	+	
30" M	26'	+25			
14" M	26'	22+12			
			9.5'		
			10'		
36" M	26'	+94	12.5'		
				grav	
				8" Corr	
				Conc. Hd w/s	
				H	
± P.L.	+40	+44	± 60'		
15" Ap	27'	+20			
		21+14	26'		shrub
		+96	30'		±
		+96	19.5'	+	
		20+95	24'		± End fruit trees

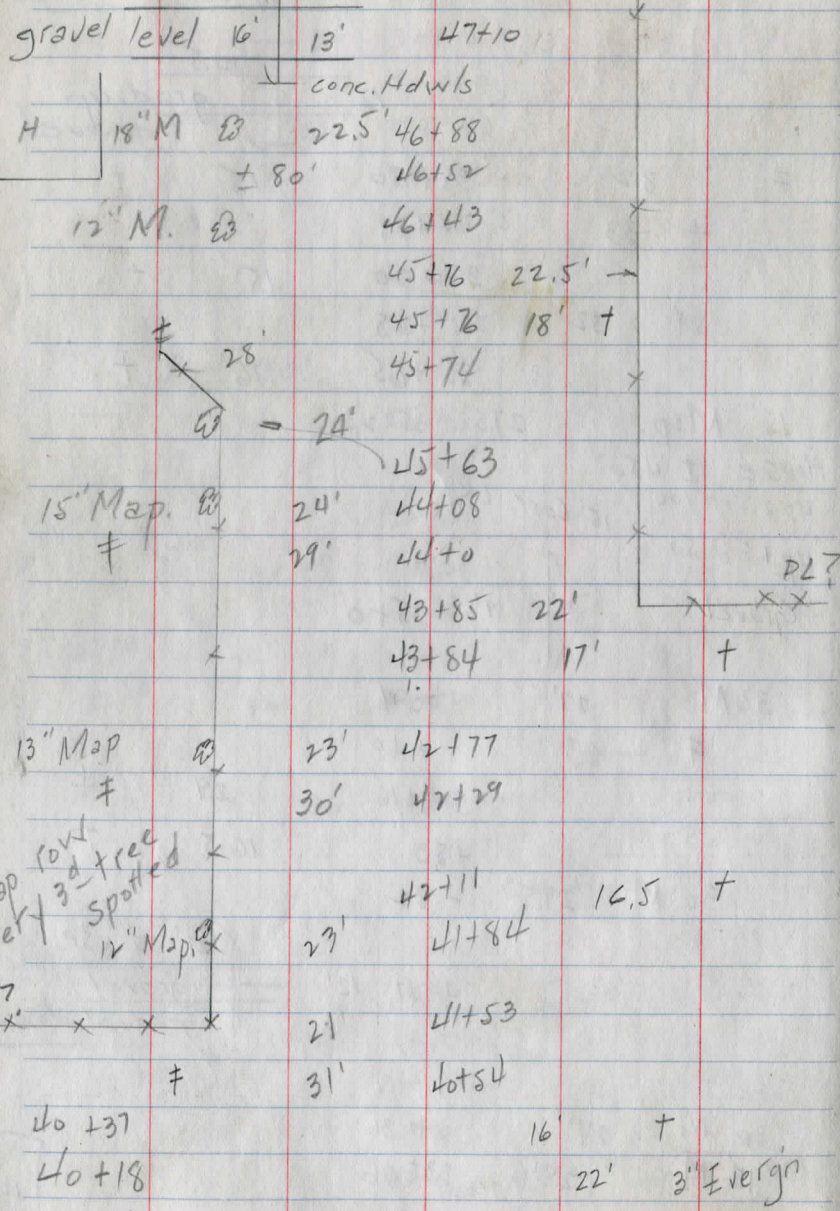


		39+50	± 180'	H
			15" Corr. Ho good	
			14.5'	
			grad. up	
			gravel	
±	32	38+80	15'	+
±	33	+38		
		37+20	15'	+
±	32	+88		
		35+65	16'	+
15" Map.	27.5'	35+23		
House ± 450'				
up 2.5 in 100				
up 1.5 in 50				15" Corr. OK
Gravel	18'	19'	35+0	
30" M	27'	+57		
±	33	+40		
		34+16	29'	±
		+83	16.5'	+
30" M	27.5'	+82		
		+47	12'	
			21' 8" VSP.	
			gravel	
			gradual down	
30" M	27'	+36		
15" M	28'	33+06		
30" M	28'	32+90		
		32+50		
			± 250'	H

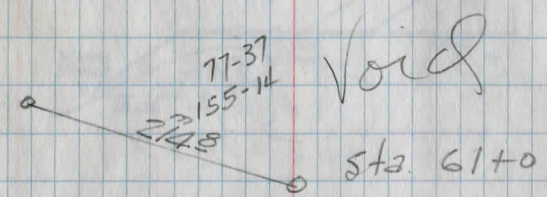


1163.34

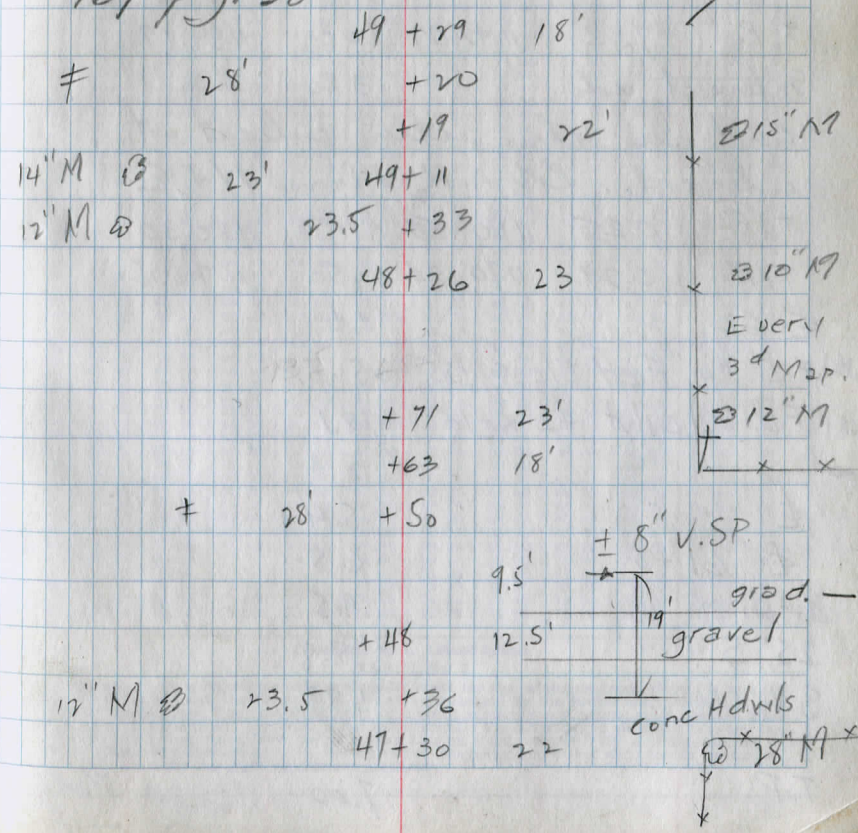
15" Corr OK
← 10' →



East
↑
E



Cont'd in Field Book No
167 pg. 38



Sta 0 is 10' W of E headwell
 X at 20 - 25⁰⁵³ + Δ
 R = 12
 T = 109.7

BM.	5.75	1179.38		1173.63	Step Stake
T.P.	6.22	1185.20	0.40	1178.98	
T.P.	7.92	1192.09	1.03	1184.17	
Intersect ads.			3.80		
Can't see thru either culvert at intersect. Lots of H ₂ O from N4 E					
T.P.	0.25	1180.55	11.79	1180.30	
T.P.	0.29	1170.34	10.50	1170.05	
£ 62			4.4		
cutlet F.L. ± 4" Field tile		61+85, 30'S	8.3		
inlet F.L. rd culvt		42" x 10"	8.1		
cut " " "			8.3		
£ " "			5.4		
£ 61+0			6.8		
S. ditch " "			9.5		
25' S " "			8.8		
BM		5.79			

T.P. 7.00 1163.34 Stake in field

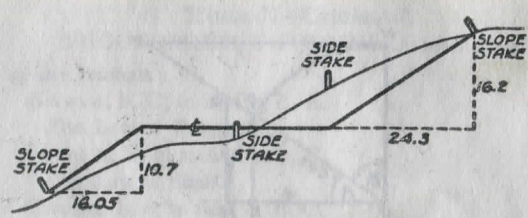


TABLE I.—DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING
 SLOPE 1 1/4 TO 1. ROADWAY OF ANY WIDTH

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0.00	0.15	0.30	0.45	0.60	0.75	0.90	1.05	1.20	1.35	0
1	2.50	1.65	1.80	1.95	2.10	2.25	2.40	2.55	2.70	2.85	1
2	3.00	3.15	3.30	3.45	3.60	3.75	3.90	4.05	4.20	4.35	2
3	4.50	4.65	4.80	4.95	5.10	5.25	5.40	5.55	5.70	5.85	3
4	6.00	6.15	6.30	6.45	6.60	6.75	6.90	7.05	7.20	7.35	4
5	7.50	7.65	7.80	7.95	8.10	8.25	8.40	8.55	8.70	8.85	5
6	9.00	9.15	9.30	9.45	9.60	9.75	9.90	10.05	10.20	10.35	6
7	10.50	10.65	10.80	10.95	11.10	11.25	11.40	11.55	11.70	11.85	7
8	12.00	12.15	12.30	12.45	12.60	12.75	12.90	13.05	13.20	13.35	8
9	13.50	13.65	13.80	13.95	14.10	14.25	14.40	14.55	14.70	14.85	9
10	15.00	15.15	15.30	15.45	15.60	15.75	15.90	16.05	16.20	16.35	10
11	16.50	16.65	16.80	16.95	17.10	17.25	17.40	17.55	17.70	17.85	11
12	18.00	18.15	18.30	18.45	18.60	18.75	18.90	19.05	19.20	19.35	12
13	19.50	19.65	19.80	19.95	20.10	20.25	20.40	20.55	20.70	20.85	13
14	21.00	21.15	21.30	21.45	21.60	21.75	21.90	22.05	22.20	22.35	14
15	22.50	22.65	22.80	22.95	23.10	23.25	23.40	23.55	23.70	23.85	15
16	24.00	24.15	24.30	24.45	24.60	24.75	24.90	25.05	25.20	25.35	16
17	25.50	25.65	25.80	25.95	26.10	26.25	26.40	26.55	26.70	26.85	17
18	27.00	27.15	27.30	27.45	27.60	27.75	27.90	28.05	28.20	28.35	18
19	28.50	28.65	28.80	28.95	29.10	29.25	29.40	29.55	29.70	29.85	19
20	30.00	30.15	30.30	30.45	30.60	30.75	30.90	31.05	31.20	31.35	20
21	31.50	31.65	31.80	31.95	32.10	32.25	32.40	32.55	32.70	32.85	21
22	33.00	33.15	33.30	33.45	33.60	33.75	33.90	34.05	34.20	34.35	22
23	34.50	34.65	34.80	34.95	35.10	35.25	35.40	35.55	35.70	35.85	23
24	36.00	36.15	36.30	36.45	36.60	36.75	36.90	37.05	37.20	37.35	24
25	37.50	37.65	37.80	37.95	38.10	38.25	38.40	38.55	38.70	38.85	25
26	39.00	39.15	39.30	39.45	39.60	39.75	39.90	40.05	40.20	40.35	26
27	40.50	40.65	40.80	40.95	41.10	41.25	41.40	41.55	41.70	41.85	27
28	42.00	42.15	42.30	42.45	42.60	42.75	42.90	43.05	43.20	43.35	28
29	43.50	43.65	43.80	43.95	44.10	44.25	44.40	44.55	44.70	44.85	29
30	45.00	45.15	45.30	45.45	45.60	45.75	45.90	46.05	46.20	46.35	30
31	46.50	46.65	46.80	46.95	47.10	47.25	47.40	47.55	47.70	47.85	31
32	48.00	48.15	48.30	48.45	48.60	48.75	48.90	49.05	49.20	49.35	32
33	49.50	49.65	49.80	49.95	50.10	50.25	50.40	50.55	50.70	50.85	33
34	51.00	51.15	51.30	51.45	51.60	51.75	51.90	52.05	52.20	52.35	34
35	52.00	52.15	52.30	52.45	52.60	52.75	52.90	53.05	53.20	53.35	35
36	54.00	54.15	54.30	54.45	54.60	54.75	54.90	55.05	55.20	55.35	36
37	55.50	55.65	55.80	55.95	56.10	56.25	56.40	56.55	56.70	56.85	37
38	57.00	57.15	57.30	57.45	57.60	57.75	57.90	58.05	58.20	58.35	38
39	58.50	58.65	58.80	58.95	59.10	59.25	59.40	59.55	59.70	59.85	39
40	60.00	60.15	60.30	60.45	60.60	60.75	60.90	61.05	61.20	61.35	40
41	61.50	61.65	61.80	61.95	62.10	62.25	62.40	62.55	62.70	62.85	41
42	63.00	63.15	63.30	63.45	63.60	63.75	63.90	64.05	64.20	64.35	42
43	64.50	64.65	64.80	64.95	65.10	65.25	65.40	65.55	65.70	65.85	43
44	66.00	66.15	66.30	66.45	66.60	66.75	66.90	67.05	67.20	67.35	44
45	67.50	67.65	67.80	67.95	68.10	68.25	68.40	68.55	68.70	68.85	45
46	69.00	69.15	69.30	69.45	69.60	69.75	69.90	70.05	70.20	70.35	46
47	70.50	70.65	70.80	70.95	71.10	71.25	71.40	71.55	71.70	71.85	47
48	72.00	72.15	72.30	72.45	72.60	72.75	72.90	73.05	73.20	73.35	48
49	73.50	73.65	73.80	73.95	74.10	74.25	74.40	74.55	74.70	74.85	49
50	75.00	75.15	75.30	75.45	75.60	75.75	75.90	76.05	76.20	76.35	50

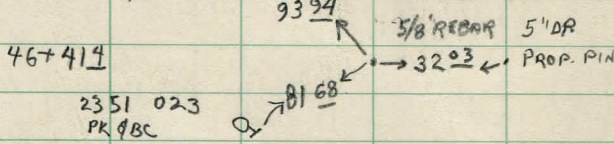
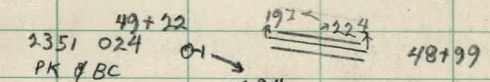
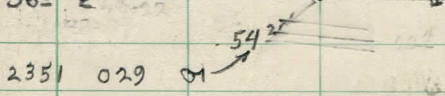
Computed by L. Leland Locke.
 TABLE No. 1

Distance of slope stake from side or shoulder stake for any width roadway, slope 1 1/4 to 1. If ground is nearly level, the cut or fill at side stake is located by the double entry method in left column and top row. The number in body of table in same row and column gives distance from side stake to slope stake. If ground is not level estimate the difference in elevation between the side stake and slope stake, lower target by this amount if cut, elevate if fill. Add this amount to cut or fill and find distance in table. Set up rod at this point, and line of sight should cut target. If it does not make the slight adjustment necessary.

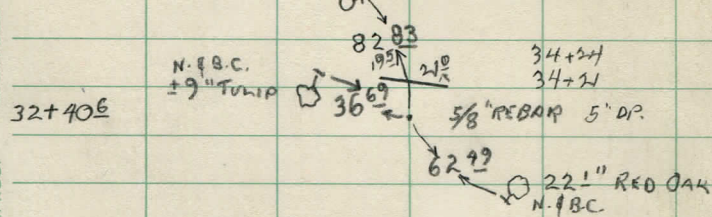
R.E. HERSHBERGER
G.A. MOHNACSKY
G.L. KOVACH
D.W. SEWELL

T.R. 49 SEC. E MOSELY RD.
LOCATION
LEDGE RD. E. TO SIOLEY RD.
10599 ← → 3984

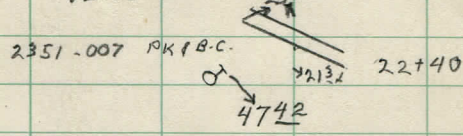
JULY - AUGUST 1982
5/8" REBAR SET 14 JULY 1982 60"
SIOLEY RD.



2351 017

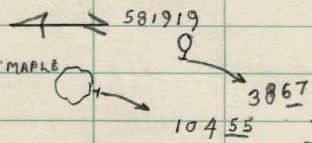


22+63

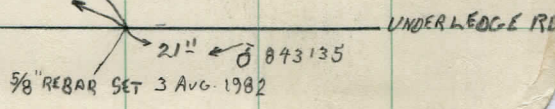


PK 7 B.C.
3.5" PEAR

13+08±



0+00



J.L. DARLINS CORP.
TACOMA, WASH. U.S.A.
Weatherproof

No. 312

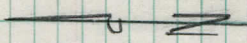
1/4 Sec. E

Bob Mosie
Don Kasie
Bob Dulice

Mosley Rd & Location

Ledge Rd East to Sidley Rd

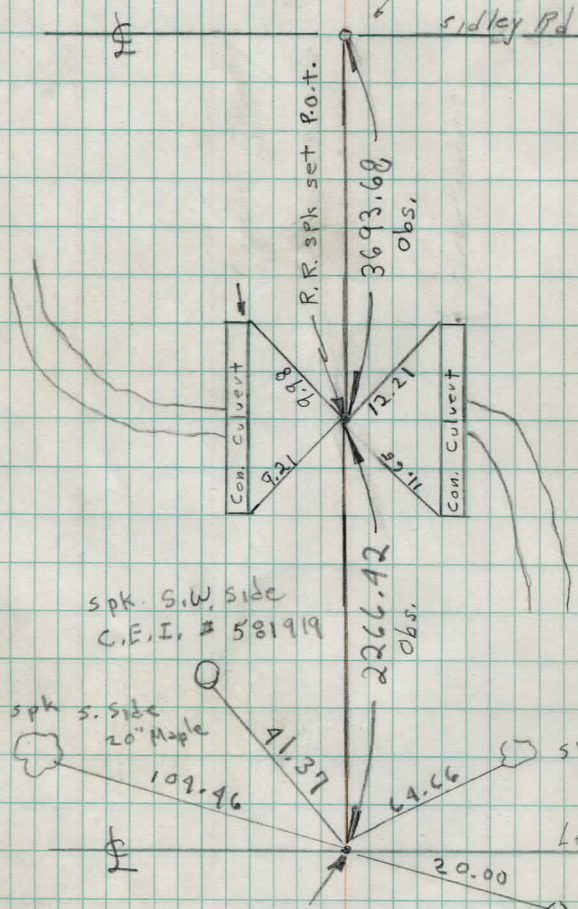
4/68



I. Pipe Fnd. + used (Bent)

see F.B. 318 pg 3

Sidley Rd



spk. S.W. side
C.E.I. # 581919

spk S. side
20" Maple
102.46

spk N.W. side
18" Maple
64.66

Ledge Rd

I. Pipe Fnd 4/68

spk N.E. side
Tele pole

